# Asymptotic preserving IMEX finite volume schemes for low Mach number Euler equations with gravitation.

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#### Abstract

In this paper we will present and analyse a new class of the IMEX finite volume schemes for the Euler equations with a gravity source term. We will in particular concentrate on a singular limit of weakly compressible flows when the Mach number  $M \ll 1$ . In order to efficiently resolve slow dynamics we split the whole nonlinear system in a stiff linear part governing the acoustic and gravity waves and a non-stiff nonlinear part that models nonlinear advection effects. For time discretization we use a special class of the so-called globally stiffly accurate IMEX schemes and approximate the stiff linear operator implicitly and the non-stiff nonlinear operator explicitly. For spatial discretization the finite volume approximation is used with the central and Rusanov/Lax-Friedrichs numerical fluxes for the linear and nonlinear subsystem, respectively. In the case of a constant background potential temperature we prove theoretically that the method is asymptotically consistent and asymptotically stable uniformly with respect to small Mach number. We also analyse experimentally convergence rates in the singular limit when the Mach number tends to zero.

Key words: finite volume methods, weakly compressible flows, low Mach number flows, IMEX schemes, asymptotic preserving schemes, asymptotic stability, multiscale analysis

AMS Subject Classification: 35L65, 76B15, 65M08, 65M06, 35L45, 35L65

# 1 Introduction

In this paper we present new asymptotic preserving implicit-explicit (IMEX) finite volume (FV) schemes for the Euler equations with gravitation. In the case of weakly compressible flows the magnitude of flow velocity **u** is much smaller than the sound speed c, which results in the socalled low Mach number flows. Here the Mach number is a reference number defined as  $M = \frac{|\mathbf{u}|}{c}$ . Such flows arise in many applications, such as meteorology, combustion or astrophysics. We refer also to theoretical works on singular limits of compressible flows, cf. [30, 18, 19]. Development of efficient and stable numerical schemes for weakly compressible flows is a challenging task. In the literature we can find already several studies on this topic. In [6] Bijl and Wesseling have developed a scheme suitable to compute large range of Mach numbers which is based on the finite difference MAC-type scheme for incompressible Euler equations. This approach has been further generalized in [26] and a conservative scheme using the pressure-correction and staggered grid approach (as in the case of the MAC scheme) has been derived and analysed. Another approach, where a numerical scheme for incompressible flows, the so-called SIMPLE

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method, has been extended to weakly compressible flows, has been developed by Munz, Roller, Klein and Geratz in [41]. In this work the formal asymptotic analysis with respect to small Mach number has been used to gain insight into the limit behavior of the compressible flow equations as the Mach number vanishes. Consequently, multiple pressure variables are introduced into the numerical framework, which allowed accurate capturing of various physical phenomena on very different length scales, see also [45] for further developments. Recently, there has been an interesting approach to approximate all Mach numbers flows derived by Feistauer et al. [20, 21], that is based on the higher order discontinuous Galerkin method. We refer also to a large variety of the so-called sound-proof models, that are used for low Mach number atmospheric flows, see, e.g., Klein et al. [35], Smolarkiewicz et al. [49], Benacchio et al. [5] and the references therein. These models suppress sound waves entirely and provide good approximations for small- to meso-scale atmospheric motions.

On the other hand, there are approaches that generalize numerical schemes developed for compressible flows in order to obtain accurate and stable methods for weakly compressible flows, see, e.g., [31, 25, 17, 8, 46, 42]. Inspired by these works, in our recent paper [43] we have split the flux into the stiff/non-stiff parts and applied implicit/explicit time discretization, that yields a nonlinear elliptic equation for the pressure updates. This acts similarly to a classical incompressible pressure projection algorithm. Unfortunately, the Jacobian of the stiff flux function degenerated in the limit as the Mach number approached zero and a suitable stabilization was needed. Thus, it implied that the spatial and the temporal grid sizes,  $\Delta x$  and  $\Delta t$ , had to be reduced simultaneously as the Mach number  $M \rightarrow 0$ . Consequently, the resulting scheme was only weakly asymptotic preserving. The concept of the so-called asymptotic preserving schemes has been introduced by Jin et al., see [25], [28] and the references therein; a numerical scheme is called asymptotic preserving if it is uniformly consistent as a singular limit parameter, e.g. the Mach number, approaches its limit. In particular, the scheme reduces to a consistent approximation of the limit equation. We recall that the semi-implicit time discretization has been also used in meteorological applications, see, e.g., [23], [46], [49], [51] to name just a few.

The aim of our paper is to present and analyse new IMEX FV schemes for the Euler equations with the gravity source that are based on acoustic/advection splitting strategy. More precisely, we split the whole nonlinear system of the Euler equations into a stiff linear part governing fast acoustic and gravity waves and a non-stiff nonlinear part that models slow nonlinear advection effects, see also our recent papers [7, 8, 9, 40]. For time discretization we use higher order globally stiffly accurate IMEX schemes and approximate the stiff linear operator implicitly and the non-stiff nonlinear operator explicitly. Consequently, we can efficiently resolve slow nonlinear dynamics due to advection effects. Our goal is to study asymptotic preserving properties of these methods and to show that a suitable splitting into the linear stiff subsystem for acoustic/gravity waves and the nonlinear non-stiff subsystem for the advection combined with the IMEX FV discretization yields asymptotic preserving schemes. In a particular case when the background potential temperature is constant, we will prove their asymptotic consistency that holds uniformly with respect to M. For the Euler equations without the gravitational source term we also prove asymptotic stability of the IMEX FV methods. Furthermore, we analyse experimentally the asymptotic convergence rates in the singular limit as  $M \to 0$  and demonstrate that our IMEX FV schemes become consistent discretizations of the limiting equations for anelastic equations in the limit of  $M \to 0$ . We also refer to a recent work of Kaiser et al.[29], where asymptotic consistency of the so-called RS IMEX schemes for the isentropic Euler equations has been studied. Note that RS IMEX schemes are strongly related to our IMEX FV schemes; both IMEX methods use analogous splitting and may differ in the choice of a reference solution or an equilibrium solution. In [7, 8] we have analysed asymptotic consistency and accuracy of the IMEX FV for the shallow water equations with a bottom topography source term.

In order to preserve equilibria of the underlying hyperbolic balance laws on the discrete level a special treatment of zero-order source terms is required, which yields the well-balanced schemes, see, e.g., [10], [4], [11], [37]. In context of the Euler equations with the gravity source term we refer a reader to Botta et al. [10], where the concept of the so-called hydrostatic reconstruction has been firstly proposed; see also [12], [13]. The schemes presented in our paper are well-balanced. Indeed, they preserve a particular underlying equilibrium by the construction, cf. Remark 5.5.

The paper is organized in the following way. In Section 2 we present the mathematical model for weakly compressible flows. The IMEX FV schemes based on a suitable splitting of linearized acoustic waves and the nonlinear advection are introduced in Section 3. In Sections 4 and 5 we study asymptotic preserving properties of our IMEX schemes; we show that they are asymptotically consistent and asymptotically stable with respect to the Mach number M. Numerical experiments presented in Section 6 demonstrate asymptotic preserving properties of the IMEX FV schemes based on the acoustic/advection splitting.

# 2 Euler equations

Time evolution of three-dimensional inviscid compressible flows is governed by the Euler equations, which express the basic conservation laws: conservation of mass, momentum and energy. In atmospheric applications it is often more suitable to express the energy equation in terms of the potential temperature, see, e.g., [5], [22], [32], [33], [36], [42], [49], [52], and the references therein. We note that for smooth flows both formulations are equivalent.

$$\partial_t \rho + \nabla \cdot (\rho \mathbf{u}) = 0$$
  
$$\partial_t (\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) + \nabla p = -\rho g \mathbf{e}_3 \equiv -\rho g \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}$$
  
$$\partial_t (\rho \theta) + \nabla \cdot (\rho \theta \mathbf{u}) = 0,$$
 (1)

where  $\rho$  denotes the density, **u** velocity vector, *p* pressure and *g* the gravitational acceleration. Equation (1)<sub>3</sub> may also be interpreted as the first law of thermodynamics for an adiabatic fluid. Denoting *T* the temperature, the potential temperature  $\theta$  can be obtained from the equation of an adiabatic process in an ideal gas

$$\theta = T\left(\frac{p_0}{p}\right)^{R/c_p}, \ R = c_p - c_v$$
 is the specific gas constant.

In order to close the system we determine the pressure from the state equation

$$p = p_0 \left(\frac{R\rho\theta}{p_0}\right)^{\gamma},\tag{2}$$

where  $\gamma = c_p/c_v$  is the adiabatic constant and  $p_0 = 10^5 Pa$  is a given reference pressure at sea level.

In practical applications there is often an underlying equilibrium background state and the dynamics of interest is governed by (small) perturbations of this equilibrium state. For example, in meteorological applications it is the hydrostatic equilibrium that expresses a balance between the gravity and pressure forces. Let  $\bar{p}$ ,  $\bar{\rho}$ ,  $\bar{\mathbf{u}}(=0)$ ,  $\bar{\theta}$ ,  $\bar{\rho\theta}$  denote the pressure, density, velocity, potential temperature and energy for the hydrostatic equilibrium, i.e.

$$\partial_{x_3}\bar{p} = -\bar{\rho}g. \tag{3}$$

Furthermore, let  $\rho', p', \mathbf{u}', \theta', (\rho\theta)'$  stand for the corresponding perturbations of the background states. Thus, we have  $\rho = \bar{\rho} + \rho', p = \bar{p} + p', \theta = \bar{\theta} + \theta'$ , and  $(\rho\theta) = \overline{\rho\theta} + \bar{\rho}\theta' + \rho'\bar{\theta} + \rho'\theta' \equiv \overline{\rho\theta} + (\rho\theta)'$ . Since with the background state  $\bar{\mathbf{u}} = 0$ , the velocity  $\mathbf{u} = \bar{\mathbf{u}} + \mathbf{u}'$  ( $\mathbf{u} \in \mathbb{R}^3$ ) becomes  $\mathbf{u} \equiv \mathbf{u}'$ , we will omit the prime symbol hereinafter.

In order to avoid numerical instabilities due to the round-off errors and the multiscale behaviour of the Euler equations in the case of low Mach number limit, the numerical simulations are typically realized for the perturbations, which satisfy the following equations

$$\partial_t \rho' + \nabla \cdot (\rho \mathbf{u}) = 0$$
  

$$\partial_t (\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) + \nabla p' = -\rho' g \mathbf{e}_3$$
  

$$\partial_t (\rho \theta)' + \nabla \cdot (\rho \theta \mathbf{u}) = 0.$$
(4)

The Pressure perturbation p' can be expressed from the state equation (2), i.e.  $p' = p - \bar{p} = p_0 \left(\frac{R}{p_0}\right)^{\gamma} ((\rho \theta)^{\gamma} - (\overline{\rho \theta})^{\gamma}).$ 

We apply the standard non-dimensionalisation with a reference length  $x_{ref}$ , time scale  $t_{ref}$ , reference flow velocity  $u_{ref}$ , reference density  $\rho_{ref}$  and reference pressure  $p_{ref}$ . Let the reference sound speed  $c_{ref} := \sqrt{\gamma p_{ref}/\rho_{ref}}$  and  $u_{ref}t_{ref} = x_{ref}$ . Then the Mach and Froude numbers read

$$M = \frac{u_{ref}}{c_{ref}}, \quad Fr = \frac{u_{ref}}{\sqrt{gx_{ref}}}.$$
(5)

We assume that  $\gamma M^2 = Fr^2$ . Denoting a small parameter  $\varepsilon = \sqrt{\gamma}M = Fr$ , the Euler equations for the perturbed variables (4) can be rewritten equivalently in the non-dimensional form

$$\partial_t \rho' + \nabla \cdot (\rho \mathbf{u}) = 0$$
  
$$\partial_t (\rho \mathbf{u}) + \nabla \cdot (\rho \mathbf{u} \otimes \mathbf{u}) + \frac{1}{\varepsilon^2} \nabla p' = -\frac{1}{\varepsilon^2} \rho' \mathbf{e}_3$$
  
$$\partial_t (\rho \theta)' + \nabla \cdot (\rho \theta \mathbf{u}) = 0.$$
 (6)

In the above non-dimensionalization procedure we have considered only one type of gravity waves, that are called the external (barotropic) gravity waves in the meteorological literature. In more detailed atmospheric models the internal gravity waves have to be considered as well. This yields another characteristic number, the internal Froude number  $Fr_{int} = Fr \frac{1}{\sqrt{x_{ref}\partial_{x_3}\theta/\theta}}$ ;  $M \approx Fr \ll Fr_{int} \ll 1$ . We refer a reader to [34], where a nice overview of various sound-proof models used in the meteorological literature and detailed asymptotic analysis are presented, see also [32], [33], [35].

**Remark 2.1** Let the background potential temperature be  $\bar{\theta} = \text{const.}$  and the background density at sea level be  $\bar{\rho}(0) \equiv \rho_0 = p_0/R\bar{\theta}$ . Then we have an explicit expression for the background hydrostatic equilibrium state

$$\bar{\rho}(x_3) = \frac{1}{\bar{\theta}} \left( 1 - \frac{(\gamma - 1)x_3}{\gamma \bar{\theta}} \right)^{\frac{1}{\gamma - 1}}, \quad \bar{p}(x_3) = (\bar{\rho}(x_3)\bar{\theta})^{\gamma}.$$

Indeed, using the non-dimensional form of (3),  $\bar{p}_{x_3} = \bar{\rho}$ , and the state equation  $\bar{p} = (\overline{\rho\theta})^{\gamma}$  we have the following ordinary differential equation

$$(\overline{\rho}\overline{\theta})^{\gamma-1}\frac{d(\overline{\rho}\overline{\theta})}{dx_3} = -\frac{1}{\gamma}\overline{\rho}$$
(7)

with  $\bar{\rho}(0) = \rho_0$ . Since  $\bar{\theta} = const.$  we obtain the ordinary differential equation for density

$$\frac{\theta^{\gamma}}{\gamma-1}\frac{d\rho^{\gamma-1}}{dx_3} = \bar{\theta}^{\gamma}\bar{\rho}^{\gamma-2}\frac{d\bar{\rho}}{dx_3} = -\frac{1}{\gamma},\tag{8}$$

which has a unique solution

$$\bar{\rho} = \frac{1}{\bar{\theta}} \left( 1 - \frac{(\gamma - 1)x_3}{\gamma \bar{\theta}} \right)^{\frac{1}{\gamma - 1}}.$$

The background state for pressure is obtained from the non-dimensional form of the state equation  $\bar{p} = (\bar{\rho}\bar{\theta})^{\gamma}$ . This result can be generalized also for stratified potential temperature, i.e. nonconstant  $\bar{\theta}$  with  $\frac{1}{\bar{\theta}}\frac{d\bar{\theta}}{dx_3} = \mathcal{O}(\varepsilon^2)$ . The hydrostatic distribution for  $\bar{\rho}(x_3)$  and  $\bar{p}(x_3)$  then reads [33]

$$\bar{\rho}(x_3) = \frac{1}{\bar{\theta}(x_3)} \left( 1 - \frac{\gamma - 1}{\gamma} \int_0^{x_3} \frac{1}{\bar{\theta}(z)} dz \right)^{\frac{1}{\gamma - 1}}, \qquad \bar{p}(x_3) = \left( \bar{\rho}(x_3) \bar{\theta}(x_3) \right)^{\gamma}.$$

**Remark 2.2** Using the dimensional formulation the above background hydrostatic equilibrium reads

$$\bar{\rho} = \frac{p_0}{R\bar{\theta}} \pi_e^{\frac{1}{\gamma-1}}, \qquad \bar{p} = p_0 \left(\frac{R\overline{\rho\theta}}{p_0}\right)^{\gamma}, \tag{9}$$

where  $\pi_e = 1 - g/(c_p \int_0^{x_3} \frac{1}{\theta(z)} dz)$  is the so-called Exner pressure.

**Remark 2.3** In order to analyse multiscale effects of the underlying equations it is often advisable to apply a formal asymptotic analysis and express all variables in the form of the Hilbert expansion

$$f = f^{(0)} + \varepsilon f^{(1)} + \varepsilon^2 f^{(2)}.$$
(10)

We substitute this expansion into a non-dimensional form of the Euler equations (1) and compare the equal order terms in  $\varepsilon$ . Assuming that  $\theta^{(0)} = \text{const.}$  the limit equations of (6) read

$$\nabla \cdot (\rho^{(0)} \mathbf{u}^{(0)}) = 0, \quad \partial_t (\rho^{(0)} \mathbf{u}^{(0)}) + \nabla \cdot \left(\rho^{(0)} \mathbf{u}^{(0)} \otimes \mathbf{u}^{(0)}\right) + \nabla p^{(2)} = -\rho^{(2)} \mathbf{e}_3, \tag{11}$$

$$\partial_t \theta^{(2)} + \mathbf{u}^{(0)} \cdot \nabla \theta^{(2)} = 0, \tag{12}$$

which are the incompressible Euler equations for fluids with variable density and the transport equation for potential temperature. Note that in the case of hydrostatic equilibrium state we obtain using (3) and (1)  $\bar{\rho} = \rho^{(0)}, \bar{p} = p^{(0)}, \bar{\theta} = \theta^{(0)}, \rho' = \varepsilon^2 \rho^{(2)}, p' = \varepsilon^2 p^{(2)}, \theta' = \varepsilon^2 \theta^{(2)}.$ 

Following [31], [52], [19] we can rewrite the momentum equation (11) as

$$\partial_t \mathbf{u}^{(0)} + \mathbf{u}^{(0)} \cdot \nabla \mathbf{u}^{(0)} + \frac{1}{\rho^{(0)}} \nabla p^{(2)} = \theta^{(2)} \mathbf{e}_3.$$
(13)

In the meteorological literature equations  $(11)_1$ , (13), (12) are called the anelastic model equations, see Ogura and Philipps [44].

## 3 Numerical schemes

Our asymptotic preserving FV schemes are based on the following acoustic/advection splitting of the Euler equations into a linear  $\mathcal{L}$  and nonlinear  $\mathcal{N}$  part, respectively, see also [46], [40] and the references therein for further details. To this end let us rewrite (4) in the following compact form. Let  $\mathbf{w} = (\rho', \rho \mathbf{u}, \rho \theta')^T$ ,  $\mathbf{F} = (\rho \mathbf{u}, \rho \mathbf{u} \otimes \mathbf{u} + \frac{1}{\varepsilon^2} p' \mathbb{1}, \rho \theta \mathbf{u})^T$ ,  $\mathbb{1} \in \mathbb{R}^{3 \times 3}$  is the identity matrix,  $S = (0, -\frac{1}{\varepsilon^2} \rho' \mathbf{e}_3, 0)^T$ , then (6) can be written as

$$\frac{\partial \mathbf{w}}{\partial t} = -\nabla \cdot \mathbf{F}(\mathbf{w}) + \mathbf{S}(\mathbf{w}) = \mathcal{L}(\mathbf{w}) + \mathcal{N}(\mathbf{w}).$$
(14)

We would like to point out that the choice of the linear and nonlinear operators,  $\mathcal{L}$  and  $\mathcal{N}$ , respectively, is crucial. Indeed, we choose  $\mathcal{L}$  to model linear acoustic and gravity waves, whereas the operator  $\mathcal{N}$  describes resulting nonlinear advective/convective effects. Analogously as in [40] we set

$$\mathcal{L}(\mathbf{w}) \equiv -\nabla \cdot \mathcal{F}_L(\mathbf{w}) + S(\mathbf{w}) := - \begin{pmatrix} \nabla \cdot (\rho \mathbf{u}) \\ \frac{1}{\varepsilon^2} \partial p' / \partial x_1 \\ \frac{1}{\varepsilon^2} \partial p' / \partial x_2 \\ \frac{1}{\varepsilon^2} \partial p' / \partial x_3 + \frac{1}{\varepsilon^2} \rho' \\ \nabla \cdot (\overline{\theta} \rho \mathbf{u}) \end{pmatrix}$$
(15)

with the linearized pressure  $p' \approx p'_L \equiv \frac{\bar{c}^2}{\bar{\theta}} (\rho \theta)'$  and

$$\mathcal{N} \equiv -\nabla \cdot \mathcal{F}_N(\mathbf{w}) := -\nabla \cdot \begin{pmatrix} 0 \\ \rho \mathbf{u} \otimes \mathbf{u} \\ \theta' \rho \mathbf{u} \end{pmatrix}.$$
 (16)

Realizing that  $\bar{\theta} = \overline{\rho \theta}/\bar{\rho}$  the linearized pressure  $p'_L$  has been obtained by applying the Taylor expansion in the expression for p' with respect to  $\overline{\rho \theta}$ . Thus, we have  $p' = (\rho \theta)^{\gamma} - (\overline{\rho \theta})^{\gamma}$ ,  $p' = p'_L + p'_{NL}$ , where

$$p'_{L} = \frac{\bar{c}^{2}}{\bar{\theta}}(\rho\theta)' \text{ with } \bar{c} = \sqrt{\frac{\gamma\bar{p}}{\bar{\rho}}} \text{ and } p'_{NL} = p' - p'_{L} = \mathcal{O}(((\rho\theta)')^{2}).$$
(17)

In the nonlinear operator  $\mathcal{N}$  one may also include the nonlinear pressure perturbation  $p'_{NL} = \mathcal{O}(\varepsilon^4)$ . However, in order to simplify the eigenstructure of  $\mathcal{N}$  and to keep the operator hyperbolic it is suitable to omit  $p'_{NL}$ . Our extensive numerical experiments demonstrate that both approaches with/without  $p'_{NL}$  yield similar results in the low Mach number limit. It is worthwhile to point out that the linear flux leads to the stiff subsystem

$$\frac{\partial \mathbf{w}}{\partial t} = -\nabla \cdot \mathcal{F}_L(\mathbf{w}) \tag{18}$$

having the eigenvalues  $\lambda_1 = -\frac{\bar{c}}{\varepsilon}$ ,  $\lambda_2 = \lambda_3 = \lambda_4 = 0$ ,  $\lambda_5 = \frac{\bar{c}}{\varepsilon}$ ,  $\bar{c} = \sqrt{\gamma \bar{p}/\bar{\rho}}$ . Note, that the internal gravity waves do not arise as a linear mode in our linearized analysis. The external gravity waves are treated as a source term. On the other hand the nonlinear subsystem

$$\frac{\partial \mathbf{w}}{\partial t} = -\nabla \cdot \mathcal{F}_{NL}(\mathbf{w}) \tag{19}$$

is non-stiff and its eigenvalues are  $\lambda_1 = 0, \lambda_2 = \lambda_3 = \lambda_4 = \mathbf{u} \cdot \mathbf{n}, \lambda_5 = 2\mathbf{u} \cdot \mathbf{n}$ , where  $\mathbf{n} \in \mathbb{R}^3$  is an arbitrary unit vector.

Consequently, we will discretize the Euler equations by the IMEX scheme in time and approximate the linear stiff system at a new time level  $t_{n+1}$  and the nonlinear one at the old time level  $t_n$ . This yields the first order IMEX scheme

$$\mathbf{w}^{n+1} = \mathbf{w}^n + \Delta t \mathcal{L}(\mathbf{w}^{n+1}) + \Delta t \mathcal{N}(\mathbf{w}^n).$$
(20)

In order to increase the accuracy we will apply the second order IMEX schemes. One possibility is to apply the second order BDF scheme, cf. [3], [46], [47]

$$\mathbf{w}^{n+1} = \alpha_0 \mathbf{w}^n + \alpha_1 \mathbf{w}^{n-1} \beta \mathcal{L}(\mathbf{w}^{n+1}) + \beta_0 \mathcal{N}(\mathbf{w}^n) + \beta_1 \mathcal{N}(\mathbf{w}^{n-1}),$$
(21)

 $\alpha_0 = \frac{4}{3}; \ \alpha_1 = -\frac{1}{3}; \ \beta = \frac{2}{3}\Delta t; \ \beta_0 = \frac{4}{3}\Delta t; \ \beta_1 = -\frac{2}{3}\Delta t.$ 

Another option is to apply the globally stiffly accurate second order IMEX scheme. A suitable candidate is the so-called ARS(2,2,2) scheme derived by Asher, Ruuth and Spiteri in [2].

$$\mathbf{w}^{n+1/2} = \mathbf{w}^n + \Delta t \alpha [\mathcal{L}(\mathbf{w}^{n+1/2}) + \mathcal{N}(\mathbf{w}^n)]$$
(22)  
$$\mathbf{w}^{n+1} = \mathbf{w}^n + \Delta t [\delta \mathcal{N}(\mathbf{w}^n) + (1-\delta)\mathcal{N}(\mathbf{w}^{n+1/2})] + \Delta t \alpha \mathcal{L}(\mathbf{w}^{n+1}) + \Delta t (1-\alpha)\mathcal{L}(\mathbf{w}^{n+1/2}),$$

where  $\alpha = 1 - 1/\sqrt{2}; \ \delta = 1 - 1/(2\alpha).$ 

Spatial discretization is realized by the finite volume scheme. In particular, having a regular rectangular grid we approximate the corresponding divergence operators by applying the numerical flux functions in order to approximate fluxes along the cell interfaces. Let us denote the finite difference in the  $x_1$  direction at the mesh cell  $\Omega_{i,j,m} \equiv [x_i - \Delta x_1/2, x_i + \Delta x_1/2] \times [y_j - \Delta x_2/2, y_j + \Delta x_2/2] \times [z_m - \Delta x_3/2, z_m + \Delta x_3/2]$  by  $\delta_{x_1} f_{ijm} \equiv f_{i+1/2,j,m} - f_{i-1/2,j,m}, f_{i+1/2} := (f_{i+1} + f_i)/2$ ; an analogous notation holds in the  $x_2$  and  $x_3$  directions. The finite volume discretization of the operators  $\mathcal{L}$  and  $\mathcal{N}$  yields

$$\mathcal{L}(\mathbf{w}^{\ell}) = -\sum_{i,j,m} \sum_{k=1}^{3} \frac{1}{\Delta x_k} \delta_{x_k} \mathcal{H}_L(\mathbf{w}^{\ell})_{ijm} + S(\mathbf{w}^{\ell})_{ijm}, \quad \ell = n+1, n+1/2$$
(23)  
$$\mathcal{N}(\mathbf{w}^{\ell}) = -\sum_{i,j,m} \sum_{k=1}^{3} \frac{1}{\Delta x_k} \delta_{x_k} \mathcal{H}_N(\mathbf{w}^{\ell})_{ijm}, \quad \ell = n, n-1, n+1/2,$$

where  $\mathcal{H}_L$  and  $\mathcal{H}_N$  denote suitable numerical fluxes for the linear and nonlinear operators, respectively.

For the nonlinear subsystem we have applied, e.g., the Lax-Friedrichs or the Rusanov numerical flux, but any standard numerical flux yielding a stable approximation can be used as well. For example, the Lax-Friedrichs or the Rusanov flux applied in the  $x_1$ -direction gives

$$\mathcal{H}_{N}(\mathbf{w}^{\ell})_{i+1/2,j,m} = \frac{1}{2} \left( \mathcal{F}_{N}(\mathbf{w}_{i+1,j,m}^{\ell}) + \mathcal{F}_{N}(\mathbf{w}_{i,j,m}^{\ell}) - \frac{1}{\lambda} (\mathbf{w}_{i+1,j,m}^{\ell} - \mathbf{w}_{i,j,m}^{\ell}) \right)$$
(24)

with  $\lambda = \Delta t / \Delta x_1$  for the Lax-Friedrichs scheme. For the Rusanov scheme we have  $\lambda = \max(\lambda_{\mathbf{w}_{i+1,j,m}^{\ell}}, \lambda_{\mathbf{w}_{i,j,m}^{\ell}})$ , which is the maximal local eigenvalues of the Jacobian matrix corresponding to (16), that is frozen either in the right  $\mathbf{w}_{i+1,j,m}^{\ell}$  or the left  $\mathbf{w}_{i,j,m}^{\ell}$  approximate solution. In order to keep the explicit finite volume approximation of the nonlinear subsystem stable, we need to fulfill the Courant-Friedrichs-Lewy stability condition. In our numerical experiments we have denoted by

$$CFL_u \equiv \max_{s=1,2,3} \max_{i,j,m} |(\mathbf{u}_s)_{ijm}| \frac{\Delta t}{\Delta x_s}$$
(25)

and set  $CFL_u < 0.5$  instead of the stability condition required by fully explicit schemes, i.e.

$$CFL \equiv \max_{s=1,2,3} \max_{i,j,m} (|(\mathbf{u}_s)_{ijm}| + c) \frac{\Delta t}{\Delta x_s} \le 1.$$
(26)

In case of the linear subsystem it is suitable to choose central differences, which will yield asymptotic preserving schemes, cf. Section 4,

$$\mathcal{H}_L(\mathbf{w}^\ell)_{i+1/2,j,m} = \frac{1}{2} \left( \mathcal{F}_L(\mathbf{w}_{i+1,j,m}^\ell) + \mathcal{F}_L(\mathbf{w}_{i,j,m}^\ell) \right).$$
(27)

Analogous notation holds in the  $x_2, x_3$ -directions.

Application of the central differences leads directly to the second order spatial approximation. For the nonlinear subsystem the second order spatial discretization is obtained via MUSCL-type approach using a linear reconstruction in space. We refer a reader to, e.g., [8] for further details. In what follows we will analyse the above IMEX FV schemes both from the analytical as well as experimental point of view.

### 4 Asymptotic preserving properties: consistency

The aim of this section is to analyse the asymptotic preserving properties of the derived IMEX FV schemes. We will show firstly that the schemes yield consistent approximation of the limiting equations and in the limit as  $\varepsilon \to 0$  become an approximation of the anelastic equation (43). We will confine ourselves with the IMEX first order scheme; in an analogous way the generalization for the BDF2 and ARS(2,2,2) second order schemes can be derived, see [7]. For the space discretization numerical fluxes (24) and (27) are applied for the explicit and implicit parts, respectively. Using the matrix-vector notation we can rewrite first order IMEX FV method (20), (23), (24), (27) in the following form

$$M\mathbf{W}^{n+1} = \hat{\mathbf{W}}, \quad M := \mathbb{1} + \Delta tA, \tag{28}$$

where  $1 \in \mathbb{R}^{5N \times 5N}$  denotes the identity matrix, N is the number of mesh cells,  $\mathbf{W}^{n+1} \equiv (\boldsymbol{\rho}', \mathbf{Q}_1, \mathbf{Q}_2, \mathbf{Q}_3, (\boldsymbol{\rho}\boldsymbol{\theta})')^{n+1} \in \mathbb{R}^{5N}$  the solution vector at the new time step and  $\hat{\mathbf{W}} \equiv (\hat{\boldsymbol{\rho}}', \hat{\mathbf{Q}}_1, \hat{\mathbf{Q}}_2, \hat{\mathbf{Q}}_3, (\boldsymbol{\rho}\boldsymbol{\theta})') \in \mathbb{R}^{5N}$  is the vector representing the explicit terms. Further, the matrix A is the matrix arising from the central difference approximation of the linear operator  $\mathcal{L}$  in space, cf. (27)

$$A := \begin{bmatrix} 0 & \mathfrak{D}_{x_1} & \mathfrak{D}_{x_2} & \mathfrak{D}_{x_3} & 0 \\ 0 & 0 & 0 & 0 & \frac{1}{\varepsilon^2} \mathfrak{D}_{x_1} \bar{C}^2 \bar{\Theta}^{-1} \\ 0 & 0 & 0 & 0 & \frac{1}{\varepsilon^2} \mathfrak{D}_{x_2} \bar{C}^2 \bar{\Theta}^{-1} \\ \mathbb{1}/\varepsilon^2 & 0 & 0 & 0 & \frac{1}{\varepsilon^2} \mathfrak{D}_{x_3} \bar{C}^2 \bar{\Theta}^{-1} \\ 0 & \mathfrak{D}_{x_1} \bar{\Theta} & \mathfrak{D}_{x_2} \bar{\Theta} & \mathfrak{D}_{x_3} \bar{\Theta} & 0 \end{bmatrix},$$
(29)

where  $\bar{C}^2 \in \mathbb{R}^{N \times N}$  is the diagonal matrix representing the known function  $\bar{c}^2$ . If we assume that the background potential temperature  $\bar{\theta} = \text{const.}$  we have  $\bar{\Theta}^{-1} = 1/\bar{\theta}$ , otherwise  $\bar{\Theta}^{-1} \in \mathbb{R}^{N \times N}$ is a diagonal matrix. Further,  $\mathfrak{D}_{x_s} \in \mathbb{R}^{N \times N}$  represents a block matrix arising from the central differences  $\delta_{x_s} f/(2\Delta x_s)$ , s = 1, 2, 3. We apply the Gauss elimination to reduce the system and remove the momentum from the linear equations of density and potential temperature. This yields us the following system

$$(\mathbb{1} + \Delta t^2 B) \begin{pmatrix} \boldsymbol{\rho}' \\ (\boldsymbol{\rho}\boldsymbol{\theta})' \end{pmatrix}^{n+1} = \begin{pmatrix} \hat{\boldsymbol{\rho}}' - \Delta t \nabla_h \cdot \hat{\mathbf{Q}} \\ (\widehat{\boldsymbol{\rho}\boldsymbol{\theta}})' - \Delta t \nabla_h \cdot (\bar{\boldsymbol{\Theta}}\hat{\mathbf{Q}}) \end{pmatrix},$$
(30a)

$$B := \begin{bmatrix} -\frac{1}{\varepsilon^2} \mathfrak{D}_{x_3} & -\frac{1}{\varepsilon^2} \Delta_h \bar{C}^2 \bar{\Theta}^{-1} \\ -\frac{1}{\varepsilon^2} \mathfrak{D}_{x_3} \bar{\Theta} & -\frac{1}{\varepsilon^2} \nabla_h \cdot \left( (\mathbb{1}_{3N} \otimes \bar{\Theta}) \nabla_h \bar{C}^2 \bar{\Theta}^{-1} \right) \end{bmatrix}.$$
(30b)

We have denoted by  $\Delta_h$ ,  $\nabla_h$  and  $\nabla_h$  the discrete Laplace, gradient and divergence operators, that arise from the central differences operators  $\mathfrak{D}_{x_s}$ , respectively. After computing the potential temperature and density we can evaluate the momentum explicitly

$$\mathbf{Q}_{j}^{n+1} = \hat{\mathbf{Q}}_{j} - \frac{\Delta t}{\varepsilon^{2}} \mathfrak{D}_{x_{j}} \bar{C}^{2} \bar{\Theta}^{-1} (\boldsymbol{\rho} \boldsymbol{\theta})^{\prime n+1}, \quad j = 1, 2,$$
(31a)

$$\mathbf{Q}_{3}^{n+1} = \hat{\mathbf{Q}}_{3} - \frac{\Delta t}{\varepsilon^{2}} \mathfrak{D}_{x_{3}} \bar{C}^{2} \bar{\Theta}^{-1} (\boldsymbol{\rho} \boldsymbol{\theta})^{\prime n+1} - \frac{\Delta t}{\varepsilon^{2}} \boldsymbol{\rho}^{\prime n+1}.$$
(31b)

In what follows we will assume that  $\bar{\theta} = \text{const.}$  This allows us to simplify the discrete system (30) and eliminate the density from the potential temperature equation

$$\left[\mathbb{1} - \frac{\Delta t^2}{\varepsilon^2} E\right] (\boldsymbol{\rho}\boldsymbol{\theta})^{\prime n+1} = (\hat{\boldsymbol{\rho}\boldsymbol{\theta}})^{\prime} - \Delta t \bar{\Theta} \nabla_h \cdot \hat{\mathbf{Q}} - \frac{\Delta t^2}{\varepsilon^2} \mathfrak{D}_{x_3} ((\widehat{\boldsymbol{\rho}\boldsymbol{\theta}})^{\prime} - \bar{\Theta} \hat{\boldsymbol{\rho}}^{\prime}), \tag{32}$$

where

$$E := \Delta_h \bar{C}^2 + \mathfrak{D}_{x_3}.$$

Finally, we have to solve only the elliptic equation for the discrete potential temperature  $(\rho\theta)^{n+1}$ . This can be realized by any suitable linear solver; in the numerical experiments presented below we have applied the direct solver UMFPACK [16]. Having obtained the potential temperature at the new time step we can update the momentum by (31) and the density from the eliminated equation

$$\boldsymbol{\rho}^{\prime n+1} = \hat{\boldsymbol{\rho}}^{\prime} + \bar{\Theta}^{-1}((\boldsymbol{\rho}\boldsymbol{\theta})^{\prime n+1} - (\widehat{\boldsymbol{\rho}\boldsymbol{\theta}})^{\prime}).$$
(33)

In order to further analyse the structure of the resulting linear system (32) we assume for simplicity that periodic boundary conditions are applied. Then the operator  $-\Delta_h$  is positive semi-definite and  $\mathfrak{D}_{x_3}$  is anti-symmetric. Consequently, the matrix  $\left[\mathbbm{1} - \frac{\Delta t^2}{\varepsilon^2}(\Delta_h \bar{C}^2 + \mathfrak{D}_{x_3})\right]$  is positive definite and non-singular. Thus, the matrix  $\mathbbm{1} - \frac{\Delta t^2}{\varepsilon^2}E$  is non-singular for any  $\varepsilon > 0$ . This leads us to the following lemma.

**Lemma 4.1** Let the background potential temperature  $\bar{\theta} = \text{const.}$  and the periodic boundary conditions be applied. Then the linear system (32) has a unique solution for any  $\varepsilon > 0$ .

**Lemma 4.2** For any  $\mathbf{x} \in \mathbb{R}^N$  it holds

$$\mathfrak{D}_{x_3}\bar{C}^2\mathbf{x} = \bar{C}^2\mathfrak{D}_{x_3}\mathbf{x} + (1-\gamma)\mathfrak{M}_{x_3}\mathbf{x},\tag{34}$$

where  $\mathfrak{M}_{x_3}$  denotes the block matrix arising from the average operator  $\mu_x f_i = 0.5(f_{i+1} + f_{i-1})$ in the  $x_3$ -direction.

**Proof:** Let us recall that the discrete product rule gives  $\delta_x(fg)_i = \mu_x f_i \delta_x g_i + \delta_x f_i \mu_x g_i$ , where *i* denotes an index of a mesh cell. Further we have for any  $\mathbf{x} \in \mathbb{R}^N$ 

$$\mathfrak{D}_{x_3}\bar{C}^2\mathbf{x} = \mathfrak{M}_{x_3}\bar{C}^2\mathfrak{D}_{x_3}\mathbf{x} + (\bar{C}^2)_{x_3}\mathfrak{M}_{x_3}\mathbf{x},$$

where  $(\bar{C}^2)_{x_3}$  denotes the diagonal matrix representing the function  $\partial(\bar{c}^2)/\partial x_3$ . We know due to Lemma 2.1 that  $\bar{c}^2 = \gamma \bar{\theta} - (\gamma - 1)x_3$ . Thus, we have  $(\bar{C}^2)_{x_3} = (1 - \gamma)\mathbb{1}$  and  $\mathfrak{M}_{x_3}\bar{C}^2 = \bar{C}^2$ .

Remark 4.3 We will use the following properties

- 1.  $\mathfrak{D}_{x_i}, i = 1, 2, 3$  and  $\mathfrak{M}_{x_3}$  commute and can be diagonalised (since they are circulant matrices, cf. [15])
- 2.  $\mathfrak{D}_{x_i}$ , i = 1, 2, 3, are anti-symmetric
- 3.  $\mathfrak{M}_{x_3}$  is symmetric
- 4.  $\mathfrak{D}_{x_i}, i = 1, 2$  and  $\overline{C}^2$  commute (since  $\overline{c}^2$  only depends on their vertical coordinate  $x_3$ ).

**Lemma 4.4** Under the assumptions of Lemma 4.1 we have  $Ker(E) = Ker(\nabla_h)$ , where Ker(E) and  $Ker(\nabla_h)$  denote nullspaces of E and  $\nabla_h$  operators, respectively.

**Proof:** First, we have for any  $\mathbf{x} \in \mathbb{R}^N$  that  $\mathbf{x}^T \mathfrak{D}_{x_3}^T \mathfrak{M}_{x_3} \mathbf{x} = 0$ . Indeed, realizing that  $\mathfrak{B} = \mathfrak{B}^T$  for any  $\mathfrak{B} \in \mathbb{R}^{1 \times 1}$  we get

$$\mathbf{x}^T \mathfrak{D}_{x_3}^T \mathfrak{M}_{x_3} \mathbf{x} = (\mathbf{x}^T \mathfrak{D}_{x_3}^T \mathfrak{M}_{x_3} \mathbf{x})^T = -\mathbf{x}^T \mathfrak{D}_{x_3}^T \mathfrak{M}_{x_3} \mathbf{x}.$$
 (35)

Thus, applying the discrete product rule for  $\mathfrak{D}_{x_3} \overline{C}^2 \mathbf{x}$  we obtain

$$\mathbf{x}^{T} E \mathbf{x} = -\mathbf{x}^{T} \sum_{i=1}^{3} \mathfrak{D}_{x_{i}}^{T} \bar{C}^{2} \mathfrak{D}_{x_{i}} \mathbf{x} - \mathbf{x}^{T} \mathfrak{D}_{x_{3}}^{T} (1-\gamma) \mathfrak{M}_{x_{3}} \mathbf{x} = -\sum_{i=1}^{3} \|\bar{C} \mathfrak{D}_{x_{i}} \mathbf{x}\|_{2}^{2}.$$
 (36)

This implies  $Ker(E) \subset Ker(\nabla_h)$ , since  $\overline{C}^2$  is regular. Let  $\nabla_h \mathbf{x} = 0$ , i.e.  $\mathfrak{D}_{x_i} \mathbf{x} = 0$ , i = 1, 2, 3. Then, we have

$$E\mathbf{x} = \sum_{i=1}^{3} \mathfrak{D}_{x_i} \bar{C}^2 \mathfrak{D}_{x_i} \mathbf{x} + \mathfrak{D}_{x_3} (1-\gamma) \mathfrak{M}_{x_3} \mathbf{x} + \mathfrak{D}_{x_3} \mathbf{x} = 0, \qquad (37)$$

which leads us to  $Ker(\nabla_h) \subset Ker(E)$ .

Analyzing the multiplicity of the zero eigenvalue of the matrix E we obtain the following interesting projection property.

**Lemma 4.5** Let the assumptions from Lemma 4.1 hold. Then the algebraic multiplicity of the eigenvalue zero of the matrix E equals its geometric multiplicity.

**Proof:** We have to show that  $E^2 \mathbf{x} = 0$  implies  $E \mathbf{x} = 0$ . Due to Lemma 4.4 this statement is equivalent to:  $\nabla_h E \mathbf{x} = 0$  implies  $\nabla_h \mathbf{x} = 0$ . Suppose  $\nabla_h E \mathbf{x} = 0$ . Then we have

$$0 = \mathbf{x}^T \mathfrak{D}_{x_j}^2 \sum_{i=1}^3 \mathfrak{D}_{x_i}^2 \bar{C}^2 \mathbf{x} + \mathbf{x}^T \mathfrak{D}_{x_j}^2 \mathfrak{D}_{x_3} \mathbf{x} = \sum_{i=1}^3 \mathbf{x}^T \mathfrak{D}_{x_j}^2 \mathfrak{D}_{x_i}^2 \bar{C}^2 \mathbf{x} = \sum_{i=1}^3 \|\bar{C}\mathfrak{D}_{x_j}\mathfrak{D}_{x_i}\|_2^2$$

for j = 1, 2. Thus  $\mathbf{x} \in Ker(\mathfrak{D}^2_{x_j}), j = 1, 2$ . Analogously we have

$$0 = \mathbf{x}^T \mathfrak{D}_{x_3}^2 \sum_{i=1}^3 \mathfrak{D}_{x_i}^2 \bar{C}^2 \mathbf{x} + \mathbf{x}^T \mathfrak{D}_{x_3}^3 \mathbf{x} = \sum_{i=1}^3 \left( \mathbf{x}^T \mathfrak{D}_{x_3} \mathfrak{D}_{x_i}^2 \bar{C}^2 \mathfrak{D}_{x_3} \mathbf{x} + (1 - \gamma) \mathbf{x}^T \mathfrak{D}_{x_3} \mathfrak{D}_{x_i}^2 \mathbf{x} \right)$$
$$= \sum_{i=1}^3 \| \bar{C} \mathfrak{D}_{x_3}^2 \|_2^2,$$

which implies  $\mathbf{x} \in Ker(\mathfrak{D}_{x_3}^2)$ . Since the matrices  $\mathfrak{D}_{x_i}$ , i = 1, 2, 3, are diagonalisable, the nullspaces of  $\mathfrak{D}_{x_i}^2$  and  $\mathfrak{D}_{x_i}$  are identical.

Lemma 4.6 Let the assumptions from Lemma 4.1 hold. Then, we have the projection property

$$\left(1 - \frac{\Delta t^2}{\varepsilon^2} E\right)^{-1} = \pi_{Ker(E)} + \mathcal{O}(\varepsilon^2), \tag{38}$$

where  $\pi_{Ker(E)}$  is the projection onto Ker(E) along  $\mathcal{R}(E)$ ;  $\mathcal{R}(E)$  denotes the range of the matrix E. Moreover, we also have that the limit of (38) as  $\varepsilon \to 0$  is  $\pi_{Ker(E)}$ .

**Proof:** Let  $R^{-1}ER$  be the Jordan normal form of the matrix E. Then,  $R^{-1}(\mathbb{1} - \frac{\Delta t^2}{\varepsilon^2}E)R$  is the Jordan normal form of  $(\mathbb{1} - \frac{\Delta t^2}{\varepsilon^2}E)$ . Note, that the matrix R is independent of  $\varepsilon$ . Thus, it suffices to consider the Jordan blocks

$$J = \begin{pmatrix} \lambda & 1 & 0 & \cdots & 0 \\ 0 & \lambda & 1 & & \vdots \\ \vdots & \ddots & \ddots & \ddots & 0 \\ 0 & & 0 & \lambda & 1 \\ 0 & \cdots & \cdots & 0 & \lambda \end{pmatrix},$$

where  $\lambda = 1 - (\Delta t/\varepsilon)^2 \mu$ ,  $\mu$  being an eigenvalue of E. Note that  $\lambda \neq 0$ , since  $1 - \frac{\Delta t^2}{\varepsilon^2} E$  is non-singular, cf. Lemma 4.1. Hence, we can compute the inverse of J, cf. [24, Section 9.1.1],

$$J^{-1} = \begin{pmatrix} \lambda^{-1} & -\lambda^{-2} & \cdots & \cdots & (-1)^{n-1}\lambda^{-n} \\ 0 & \lambda^{-1} & -\lambda^{-2} & \cdots & (-1)^{n-2}\lambda^{-(n-1)} \\ \vdots & \ddots & \ddots & \ddots & \vdots \\ 0 & 0 & \lambda^{-1} & -\lambda^{-2} \\ 0 & \cdots & \cdots & 0 & \lambda^{-1} \end{pmatrix}$$

We have

$$\lambda^{-1} = \frac{\varepsilon^2}{\varepsilon^2 - \Delta t^2 \mu} = \begin{cases} 1, & \text{if } \mu = 0\\ \mathcal{O}(\varepsilon^2), & \text{else.} \end{cases}$$

Consequently,  $J^{-1} = \mathcal{O}(\varepsilon^2)$  for  $\mu \neq 0$ . Due to Lemma 4.5 the Jordan blocks corresponding to the eigenvalue zero are diagonal. Hence,  $J^{-1} = \mathbb{1}$  for  $\mu = 0$ .

**Theorem 4.7** Let the assumption of Lemma 4.1 hold and  $\rho'^n$ ,  $(\rho\theta)'^n = \mathcal{O}(\varepsilon^2)$ . Then the numerical solution satisfies the following asymptotic preserving properties

$$(\rho\theta)^{\prime n+1}, \rho^{\prime n+1}, \nabla_h \cdot \mathbf{Q}^{n+1} = \mathcal{O}(\varepsilon^2), \tag{39}$$

if a numerical flux for the explicit finite volume scheme obeys the following property:

$$\rho'^n, (\rho\theta)'^n = \mathcal{O}(\varepsilon^2) \implies \hat{\rho}', (\widehat{\rho\theta})' = \mathcal{O}(\varepsilon^2).$$
 (40)

**Proof:** First, we note that (36) implies  $Ker(E^T) \subset Ker(\nabla_h) = Ker(E)$ . Since the dimensions of the kernel of E and  $E^T$  are equal, we have  $Ker(E^T) = Ker(E)$ . Consequently  $Ker(E)^{\perp} = \mathcal{R}(E)$  and the projection in (38) is the orthogonal projection on Ker(E). Further,

$$\mathcal{R}(E) = Ker(E)^{\perp} = Ker(\nabla_h)^{\perp} = \mathcal{R}(\nabla_h^T) = \mathcal{R}(\nabla_h \cdot).$$
(41)

This yields  $(\rho\theta)'^{n+1} = \pi_{Ker(E)}(\widehat{\rho\theta})' + \mathcal{O}(\varepsilon^2) = \mathcal{O}(\varepsilon^2)$ . From (33) we obtain

$$\rho'^{n+1} = \hat{\rho}' + \frac{(\rho\theta)'^{n+1} - (\rho\theta)'}{\bar{\theta}} = \mathcal{O}(\varepsilon^2).$$
(42)

From the continuity or the potential temperature equation we conclude, that  $\nabla_h \cdot \mathbf{Q}^{n+1} = \mathcal{O}(\varepsilon^2)$ .

**Remark 4.8** Let the initial data satisfy  $\rho'(0, \cdot) = \mathcal{O}(\varepsilon^2)$ ,  $(\rho\theta)'(0, \cdot) = \mathcal{O}(\varepsilon^2)$ . Then one can apply a suitable explicit finite volume method to approximate the nonlinear subsystem (19), that will preserve this property, i.e. (40). For example, the Lax-Friedrichs method used below is one possible choice.

We would like to point out that the divergence property of the momentum is controlled in our scheme only in the implicit step. For alternative approaches, where the divergence of momentum is either controlled by the extrapolation of the advective fluxes from the previous time step or by the MAC-type projection, we refer a reader to, e.g., [49].

Corollary 4.9 Let the initial data of (1) be well-prepared, i.e.

$$\rho(0,\cdot) = \bar{\rho} + \varepsilon^2 \rho^{(2)}(0,\cdot), \quad \theta(0,\cdot) = \bar{\theta} + \varepsilon^2 \theta^{(2)}(0,\cdot), \quad \bar{\theta} = const.$$

Then in the limit as  $\varepsilon \to 0$  the IMEX FV scheme yields a consistent approximation of the limiting anelastic equations

$$\nabla \cdot (\mathbf{q}^{(0)}) = 0, \quad \mathbf{q}^{(0)} \equiv \rho^{(0)} \mathbf{u}^{(0)}$$
  
$$\partial_t (\rho^{(0)} \mathbf{u}^{(0)}) + \nabla \cdot \left( \rho^{(0)} \mathbf{u}^{(0)} \otimes \mathbf{u}^{(0)} \right) + \nabla \Pi = -\rho^{(2)} \mathbf{e}_3, \qquad (43)$$
  
$$\partial_t \theta^{(2)} + \mathbf{u}^{(0)} \cdot \nabla \theta^{(2)} = 0,$$

where  $\rho^{(0)} = \bar{\rho}$ ,  $\theta^{(0)} = \bar{\theta}$ ,  $(\rho\theta)^{(2)} = \lim_{\varepsilon \to 0} \frac{(\rho\theta)'}{\varepsilon^2}$ ,  $\rho^{(2)} = \lim_{\varepsilon \to 0} \frac{\rho'}{\varepsilon^2}$ ,  $\theta^{(2)} = ((\rho\theta)^{(2)} - \rho^{(2)}\bar{\theta})/(\bar{\rho} + \rho^{(2)})$ . Further,  $\Pi$  is the pressure, the presence of which is enforced by the divergence freedom of the momentum, i.e.  $\Pi$  acts as the corresponding Lagrange multiplier.

**Proof:** follows from the fact that our IMEX FV scheme gives an asymptotic consistent approximation of the Euler equations (1) and from the formal asymptotic analysis; see also a recent result of Feireisl et al. [19], where the convergence of the solution of (1) to a smooth solution of the incompressible limit is rigorously proven.  $\Box$ 

### 5 Asymptotic preserving properties: stability

The aim of this section is to discuss asymptotic stability of our IMEX schemes. We will again concentrate on the first order IMEX FV method (20), (23), (24), (27). Applying the operator splitting approach we analyse firstly asymptotic stability of the linear subsystem, that is approximated implicitly in time and by the central differences in space.

Let us denote by  $\Omega \subset \mathbb{R}^3$  a computational domain and let  $\mathbf{w}_h^{n+1} = \left(\rho_h^{\prime n+1}, \mathbf{q}_h^{n+1}, (\rho\theta)_h^{\prime n+1}\right)$ ,  $\hat{\mathbf{w}}_h = \left(\hat{\rho}_h^{\prime}, \hat{\mathbf{q}}_h, (\widehat{\rho\theta})_h^{\prime}\right)$  be the discrete solutions of the linear subsystem (18) and the nonlinear subsystem (19), respectively. Note that  $\mathbf{w}_h^{n+1} : \Omega \to \mathbb{R}^5$  is a piecewise constant function in space, such that  $\mathbf{w}_h^{n+1}\Big|_{\Omega_{i,j,m}} \equiv \mathbf{w}_{i,j,m}^{n+1}$  for all mesh cells  $\Omega_{i,j,m}$ . Analogous notation holds for  $\hat{\mathbf{w}}_h$ . We concentrate here on the linear subsystem (18) without gravitation, the proof of asymptotic stability for the Euler equation with the gravity term is more delicate and will be considered in our forthcoming paper. Our numerical scheme for (18) can be reformulated equivalently in the following way

$$\frac{(\rho')_{h}^{n+1} - (\hat{\rho'})_{h}}{\Delta t} + \nabla_{h} \cdot \mathbf{q}_{h}^{n+1} = 0$$

$$\frac{\mathbf{q}_{h}^{n+1} - \hat{\mathbf{q}}_{h}}{\Delta t} + \frac{1}{\varepsilon^{2}\bar{\theta}} \nabla_{h} (\bar{c}_{h}^{2}(\rho\theta)')_{h}^{n+1} = 0$$

$$\frac{((\rho\theta)')_{h}^{n+1} - ((\hat{\rho\theta})')_{h}}{\Delta t} + \nabla_{h} \cdot (\mathbf{q}_{h}^{n+1}\bar{\theta}) = 0,$$
(44)

where  $\nabla_h$  and  $\nabla_h$  denotes now the finite difference operators for the discrete gradient and discrete divergence arising from the central differences  $\delta_{xs}/(2\Delta x_s)$ , s = 1, 2, 3. We will denote by  $\|\mathbf{w}_h\|$  the discrete  $L^2$ -norm, i.e.  $\|\mathbf{w}_h\|^2 = \int_{\Omega} (\mathbf{w}_h)^2 dx dy dz = \sum_{i,j,m} |\Omega_{i,j,m}| (\mathbf{w}_{i,j,m})^2$ . Here the summation is done over all indices i, j, m, such that a mesh cell  $\Omega_{i,j,m} \subseteq \Omega$  and  $|\Omega_{i,j,m}|$  denotes the volume of the corresponding mesh cell.

In what follows we assume that either periodic or no-flux boundary conditions are prescribed. In the latter case we set  $\mathbf{u} \cdot \mathbf{n} = 0$  and enforce additionally the numerical boundary conditions  $\nabla_h \bar{c}_h^2 (\rho \theta)'_h \cdot \mathbf{n} = 0 = \nabla_h \rho'_h \cdot \mathbf{n}$  for ghost cells. Thus, we extrapolate the linearized pressure and the density in the normal direction. These types of boundary conditions have been also used in our numerical experiments presented below. Analogously as in the previous section we do not consider in our stability analysis arbitrary background stratifications of potential temperature, but confine ourselves to the case of  $\bar{\theta} = const$ .

#### Theorem 5.1 (Asymptotic stability for the linear subsystem)

Let us assume that  $\bar{\theta} = \text{const.}$  and periodic or no-flux boundary conditions are used. Then the implicit finite difference approximation of the linear subsystem (15) is asymptotically stable, i.e. we have for any  $0 < \varepsilon \ll 1$ 

$$\left\|\frac{\bar{c}_h}{\varepsilon\bar{\theta}}(\rho\theta)_h^{\prime n+1}\right\| + \left\|\mathbf{q}_h^{n+1}\right\| + \left\|(\rho\theta')_h^{n+1}\right\| \le \left\|\frac{\bar{c}_h}{\varepsilon\bar{\theta}}(\widehat{\rho\theta})_h^{\prime}\right\| + \left\|\hat{\mathbf{q}}_h\right\| + \left\|\widehat{\rho\theta'}_h\right\|.$$
(45)

**Proof:** By substituting  $(15)_2$  into  $(15)_3$  we get

$$(\rho\theta)_{h}^{\prime n+1} - \left(\frac{\Delta t}{\varepsilon}\right)^{2} \nabla_{h} \cdot \left(\nabla_{h}(\bar{c}_{h}^{2}(\rho\theta)_{h}^{\prime n+1})\right) = (\widehat{\rho\theta})_{h}^{\prime} - \Delta t \nabla_{h} \cdot (\bar{\theta}\hat{\mathbf{q}}_{h}).$$
(46)

Analogously, we also have

$$(\rho')_{h}^{n+1} - \left(\frac{\Delta t}{\varepsilon}\right)^{2} \nabla_{h} \cdot \left(\nabla_{h} \left(\frac{\bar{c}_{h}^{2}}{\bar{\theta}}(\rho\theta)_{h}^{\prime n+1}\right)\right) = (\hat{\rho'})_{h} - \Delta t \nabla_{h} \cdot (\hat{\mathbf{q}}_{h}).$$
(47)

Now we multiply the equation (46) by  $\frac{\bar{c}_h^2}{\theta^2 \varepsilon^2} (\rho \theta)_h^{\prime n+1}$  and (15)<sub>2</sub> by  $\hat{\mathbf{q}}_h$ , integrating over  $\Omega$  yields

$$\frac{1}{2} \|\mathbf{q}_{h}^{n+1}\|^{2} - \frac{1}{2} \|\hat{\mathbf{q}}_{h}\|^{2} - \frac{1}{2} \|\mathbf{q}_{h}^{n+1} - \hat{\mathbf{q}}_{h}\|^{2} + \Delta t \frac{1}{\varepsilon^{2} \bar{\theta}} \int_{\Omega} \nabla_{h} \left( \bar{c}_{h}^{2} (\rho \theta)_{h}^{\prime n+1} \right) \hat{\mathbf{q}}_{h} = 0$$
(48)

$$\frac{1}{2} \left\| \frac{\bar{c}_h}{\varepsilon \bar{\theta}} (\rho \theta)_h^{\prime n+1} \right\|^2 - \frac{1}{2} \left\| \frac{\bar{c}_h}{\varepsilon \bar{\theta}} (\rho \bar{\theta})_h^{\prime} \right\|^2 + \frac{1}{2} \left\| \frac{\bar{c}_h}{\varepsilon \bar{\theta}} (\rho \theta)_h^{\prime n+1} - \frac{\bar{c}_h}{\varepsilon \bar{\theta}} (\rho \bar{\theta})_h^{\prime} \right\|^2 + \Delta t \int_{\Omega} \frac{\bar{c}_h^2}{\varepsilon^2 \bar{\theta}} (\rho \theta)_h^{\prime n+1} \nabla_h \cdot \hat{\mathbf{q}}_h + \left( \frac{\Delta t}{\varepsilon} \right)^2 \left\| \nabla_h \left( \frac{\bar{c}_h^2}{\varepsilon \bar{\theta}} (\rho \theta)_h^{\prime n+1} \right) \right\|^2 = 0,$$
(49)

where we have used the discrete integration by parts and periodic or no-flux boundary conditions. Summing (48) and (49) leads to

$$\frac{1}{2} \|\mathbf{q}_{h}^{n+1}\|^{2} - \frac{1}{2} \|\hat{\mathbf{q}}_{h}\|^{2} - \frac{1}{2} \|\mathbf{q}_{h}^{n+1} - \hat{\mathbf{q}}_{h}\|^{2} + \frac{1}{2} \left\|\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\theta)_{h}^{\prime n+1}\right\|^{2} - \frac{1}{2} \left\|\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\bar{\theta})_{h}^{\prime}\right\|^{2} + \frac{1}{2} \left\|\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\theta)_{h}^{\prime n+1} - \frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\bar{\theta})_{h}^{\prime}\right\|^{2} + \left(\frac{\Delta t}{\varepsilon}\right)^{2} \left\|\nabla_{h}\left(\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\theta)_{h}^{\prime n+1}\right)\right\|^{2} = 0.$$

$$(50)$$

From the momentum equation  $(15)_2$  we obtain

$$\frac{1}{2} \|\mathbf{q}_h^{n+1} - \hat{\mathbf{q}}_h\|^2 = \frac{1}{2} \left(\frac{\Delta t}{\varepsilon}\right)^2 \left\|\nabla_h \left(\frac{\bar{c}_h}{\varepsilon \bar{\theta}}(\rho \theta)_h^{\prime n+1}\right)\right\|^2.$$
(51)

Substituting (51) into (50) yields

$$\frac{1}{2} \|\mathbf{q}_{h}^{n+1}\|^{2} - \frac{1}{2} \|\hat{\mathbf{q}}_{h}\|^{2} + \frac{1}{2} \left\|\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\theta)_{h}^{\prime n+1}\right\|^{2} - \frac{1}{2} \left\|\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\bar{\theta})_{h}^{\prime}\right\|^{2} + \frac{1}{2} \left(\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\theta)_{h}^{\prime n+1} - \frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\bar{\theta})_{h}^{\prime}\right\|^{2} + \frac{1}{2} \left(\frac{\Delta t}{\varepsilon}\right)^{2} \left\|\nabla_{h}\left(\frac{\bar{c}_{h}^{2}}{\varepsilon\bar{\theta}}(\rho\theta)_{h}^{\prime n+1}\right)\right\|^{2} = 0$$
(52)

and we obtain

$$\begin{aligned} \|\mathbf{q}_{h}^{n+1}\|^{2} + \left\|\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\theta)_{h}^{\prime n+1}\right\|^{2} + \left\|\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\theta)_{h}^{\prime n+1} - \frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\widehat{\theta})_{h}^{\prime}\right\|^{2} + \left(\frac{\Delta t}{\varepsilon}\right)^{2} \left\|\nabla_{h}\left(\frac{\bar{c}_{h}^{2}}{\varepsilon\bar{\theta}}(\rho\theta)_{h}^{\prime n+1}\right)\right\|^{2} \\ &= \left\|\hat{\mathbf{q}}_{h}\right\|^{2} + \left\|\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\widehat{\theta})_{h}^{\prime}\right\|^{2}.\end{aligned}$$

This leads to the desired stability estimate

$$\|\mathbf{q}_{h}^{n+1}\|^{2} + \left\|\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\theta)_{h}^{\prime n+1}\right\|^{2} \leq \|\hat{\mathbf{q}}_{h}\|^{2} + \left\|\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\theta)_{h}^{\prime}\right\|^{2}.$$
(53)

We also note that the asymptotic consistency analysis presented in the previous section shows that  $\mathbf{q}_h^{n+1} = \mathcal{O}(1)$ , while  $(\rho\theta)_h^{n+1} = \mathcal{O}(\varepsilon^2) = (\rho')_h^{n+1}$ . Combining this fact with (53), which is uniform in  $\varepsilon > 0$ , yields also

$$\|\mathbf{q}_{h}^{n+1}\| \leq \|\hat{\mathbf{q}}_{h}\|, \qquad \left\|\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\rho\theta)_{h}^{\prime n+1}\right\| \leq \left\|\frac{\bar{c}_{h}}{\varepsilon\bar{\theta}}(\widehat{\rho\theta})_{h}^{\prime}\right\|.$$
(54)

Multiplying (47) by  $\bar{\theta}$  we obtain

$$(\rho\theta')_{h}^{n+1} \equiv (\rho\theta)_{h}^{\prime n+1} - \bar{\theta}(\rho')_{h}^{n+1} = (\widehat{\rho\theta})_{h}^{\prime} - \bar{\theta}\hat{\rho'}_{h} \equiv \widehat{\rho\theta'}_{h}$$
(55)

and consequently  $\|(\rho\theta')_h^{n+1}\| = \|\widehat{\rho\theta'}_h\|$ , which concludes the proof.

**Remark 5.2** Applying the triangular inequality to (55) leads to the boundedness of the density as well  $\|(\rho')_h^{n+1}\| \leq \|\hat{\rho'}_h\| + \frac{1}{\theta}\|(\hat{\rho\theta})'_h\| + \frac{1}{\theta}\|(\rho\theta)'_h^{n+1}\|$ . Combining it with (53) we obtain the following stability estimate

$$\left\|\mathbf{q}_{h}^{n+1}\right\| + \left\|\frac{\overline{c}_{h}}{\varepsilon\overline{\theta}}(\rho\theta)_{h}^{\prime n+1}\right\| + \left\|\frac{\overline{c}_{h}}{\varepsilon}(\rho')_{h}^{n+1}\right\| \leq \left\|\hat{\mathbf{q}}_{h}\right\| + 3\left\|\frac{\overline{c}_{h}}{\varepsilon\overline{\theta}}(\widehat{\rho\theta})_{h}^{\prime}\right\| + \left\|\frac{\overline{c}_{h}}{\varepsilon}\widehat{\rho'}_{h}\right\|.$$
(56)

Next, we will study stability of the nonlinear subsystem that is discretized explicitly by, e.g., the Lax-Friedrichs scheme.

$$\hat{\rho}'_{ijm} = \frac{1}{3} \left( \mu_{x_1} \rho' + \mu_{x_2} \rho' + \mu_{x_3} \rho' \right)^n_{ijm}$$

$$\hat{\mathbf{q}}_{ijm} = \frac{1}{3} \left( \mu_{x_1} \mathbf{q} + \mu_{x_2} \mathbf{q} + \mu_{x_3} \mathbf{q} \right)^n_{ijm} - \Delta t \sum_{s=1}^3 \frac{1}{2\Delta x_s} \delta_{x_s} (\mathbf{q} \mathbf{u}_s)^n_{ijm}$$

$$(57)$$

$$(\widehat{\rho \theta})'_{ijm} = \frac{1}{3} \left( \mu_{x_1} (\rho \theta)' + \mu_{x_2} (\rho \theta)' + \mu_{x_3} (\rho \theta)' \right)^n_{ijm} - \Delta t \sum_{s=1}^3 \frac{1}{2\Delta x_s} \delta_{x_s} (\rho \theta' \mathbf{u}_s)^n_{ijm}$$

In what follows, we will derive the uniform  $L^1$ -stability estimates with respect to  $\varepsilon > 0$ . To this end let us denote by  $\|\cdot\|$  the discrete  $L^1$ -norm. Using the triangular inequality, no-flux or periodic boundary conditions we obtain

$$\|\hat{\rho}_{h}\| \equiv \sum_{i,j,m} |\Omega_{ijm}| |\hat{\rho}'_{ijm}| \leq \frac{1}{6} \sum_{i,j,m} |\Omega_{ijm}| \left( |\rho'^{n}_{i+1,j,m}| + |\rho'^{n}_{i-1,j,m}| + |\rho'^{n}_{i,j+1,m}| + |\rho'^{n}_{i,j-1,m}| + |\rho'^{n}_{i,j-1,m}| + |\rho'^{n}_{i,j,m+1}| + |\rho'^{n}_{i,j,m-1}| \right) \leq \sum_{i,j,m} |\Omega_{ijm}| |\rho'^{n}_{ijm}| \equiv \|\rho'^{n}_{h}\|.$$
(58)

Applying the CFL stability condition and the periodic or no-flux boundary conditions the momentum equation  $(57)_2$  yields

$$\begin{aligned} \|\hat{\mathbf{q}}_{h}\| &\equiv \sum_{i,j,m} |\Omega_{ijm}| |\hat{\mathbf{q}}_{ijm}| \leq \\ \frac{1}{2} \sum_{i,j,m} |\Omega_{ijm}| \left| \left( \frac{1}{3} - \frac{\Delta t}{\Delta x_{1}} (\mathbf{u}_{1}^{n})_{i+1,j,m} \right) \mathbf{q}_{i+1,j,m}^{n} \right| + \left| \left( \frac{1}{3} + \frac{\Delta t}{\Delta x_{1}} (\mathbf{u}_{1}^{n})_{i-1,j,m} \right) \mathbf{q}_{i-1,j,m}^{n} \right| \\ + \frac{1}{2} \sum_{i,j,m} |\Omega_{ijm}| \left| \left( \frac{1}{3} - \frac{\Delta t}{\Delta x_{2}} (\mathbf{u}_{2}^{n})_{i,j+1,m} \right) \mathbf{q}_{i,j+1,m}^{n} \right| + \left| \left( \frac{1}{3} + \frac{\Delta t}{\Delta x_{2}} (\mathbf{u}_{2}^{n})_{i,j-1,m} \right) \mathbf{q}_{i,j-1,m}^{n} \right| \\ + \frac{1}{2} \sum_{i,j,m} |\Omega_{ijm}| \left| \left( \frac{1}{3} - \frac{\Delta t}{\Delta x_{3}} (\mathbf{u}_{3}^{n})_{i,j,m+1} \right) \mathbf{q}_{i,j,m+1}^{n} \right| + \left| \left( \frac{1}{3} + \frac{\Delta t}{\Delta x_{3}} (\mathbf{u}_{3}^{n})_{i,j,m-1} \right) \mathbf{q}_{i,j,m-1}^{n} \right| \\ = \frac{1}{2} \sum_{i,j,m} |\Omega_{ijm}| \sum_{s=1,2,3} \left[ \left( \frac{1}{3} - \frac{\Delta t}{\Delta x_{s}} (\mathbf{u}_{s}^{n})_{i,j,m} \right) + \left( \frac{1}{3} + \frac{\Delta t}{\Delta x_{s}} (\mathbf{u}_{s}^{n})_{i,j,m} \right) \right] |\mathbf{q}_{ijm}^{n}| \leq \|\mathbf{q}_{h}^{n}\|. \tag{59}$$

We would like to point out that due to the dimensional splitting arguments we have used here a slightly stronger  $CFL_u$  stability condition than (25), namely we enforce that

$$\max_{s=1,2,3} \frac{|\mathbf{u}_s| \Delta t}{\Delta x_s} \le 1/3.$$
(60)

Finally, multiplying  $(57)_1$  by  $\bar{\theta}$  and subtracting it from  $(57)_3$  we obtain the discrete evolution for  $(\rho\theta')_h$ , which is analogous to the discrete equation  $(57)_2$  for  $\mathbf{q}_h$ . Repeating the same arguments as above we obtain  $\|\widehat{\rho\theta'}_h\| \leq \|(\rho\theta')_h^n\|$ . Consequently, we have proven the following stability result.

#### Theorem 5.3 (Asymptotic stability for the nonlinear subsystem)

Let  $\bar{\theta} = \text{const.}$  and the periodic or no-flux boundary conditions are used. Let the  $CFL_u$  stability condition (60) holds. Then the explicit approximation of the nonlinear subsystem by the Lax-Friedrichs scheme is asymptotically stable, i.e. we have for any  $\varepsilon > 0$ 

$$\|\hat{\rho}_{h}'\| + \|\hat{\mathbf{q}}_{h}\| + \|\hat{\rho}\theta'_{h}\| \le \|\rho_{h}'^{n}\| + \|\mathbf{q}_{h}^{n}\| + \|(\rho\theta')_{h}^{n}\|.$$
(61)

Combing the results from Theorems 5.1, 5.3 and using the interpolation between the discrete  $L^1$  and  $L^2$ -norm, cf. [14], we finally obtain stability of our IMEX FV scheme that holds uniformly with respect to  $0 < \varepsilon \ll 1$ . Note that our stability result holds in both  $L^1$  and  $L^2$ -norms and for an arbitrary but fixed mesh and final time T > 0.

### Theorem 5.4 (Asymptotic stability of the IMEX FV scheme)

Let  $\theta = \text{const.}$  and the periodic or no-flux boundary conditions are used. We assume that the  $CFL_u$  stability condition (60) holds. Then the IMEX FV scheme (20), (23), (24), (27) for the Euler equations is asymptotically stable, i.e. we have for any  $0 < \varepsilon \ll 1$ 

$$\left\|\frac{\bar{c}_h}{\varepsilon\bar{\theta}}(\rho\theta)_h^{\prime n}\right\| + \left\|\mathbf{q}_h^n\right\| + \left\|(\rho\theta')_h^n\right\| + \left\|\frac{\bar{c}_h}{\varepsilon}(\rho')_h^n\right\| \le c(\Delta x, T)\left(\left\|\frac{\bar{c}_h}{\varepsilon\bar{\theta}}(\rho\theta)_h^{\prime 0}\right\| + \left\|\mathbf{q}_h^0\right\| + \left\|(\rho\theta')_h^0\right\| + \left\|\frac{\bar{c}_h}{\varepsilon}(\rho')_h^0\right\|\right)\right)$$

where  $(\rho_h^{\prime 0}, \mathbf{q}_h^0, (\rho \theta)_h^{\prime 0})^T$  denotes the discrete initial data and the constant  $c(\Delta x, T)$  depends on a mesh parameter  $\Delta x \equiv \max_{s=1,2,3}(\Delta x_s)$ , a final time T > 0 and a lower and upper bound of the background sound speed  $\bar{c}$ .

**Remark 5.5** (Well-balanced property) We note that our IMEX FV scheme is well-balanced by the construction. If we start with the numerical solution being in the hydrostatic equilibrium, i.e.  $\mathbf{w}^n = \mathbf{0}$ , then a new numerical solution will fulfill the same condition,  $\mathbf{w}^{n+1} = \mathbf{0}$ . Indeed, it is easy to verify that the nonlinear fluxes  $\mathcal{H}_N(\mathbf{w}^n)$ , cf. (24), vanish since  $\mathbf{w}^n = \mathbf{0}$ . Thus, the righthand side of the linear system (18) is a zero vector. Since the matrix M in (18) is non-singular, the resulting solution  $\mathbf{w}^{n+1} = \mathbf{0}$ . Thus, the hydrostatic equilibrium is preserved. Consequently, the IMEX FV is well-balanced in the sense that it preserves the hydrostatic equilibrium state, which we have started from.

### 6 Numerical experiments

In this section we present numerical results that demonstrate asymptotic preserving properties analysed above. In what follows we will use the acronyms

- EXP-RK2 for the explicit second order Runge-Kutta time discretisation and the finite volume method with the Rusanov flux for spatial discretization.
- IMEX-ARS2, cf. [2, 7], for the IMEX scheme with the ARS222 time discretisation, the finite volume method with the central differences for spatial discretization of the linear terms and the Rusanov flux for the nonlinear terms. Note that the scheme is based on the elliptic subsystem (32) instead of (18).
- IMEX-BDF2, cf. [3, 7], for the second order BDF2 scheme for time discretisation, the finite volume schemes with the central differences for spatial discretization of the linear terms and the Rusanov flux for the nonlinear terms. The scheme solves numerically the elliptic subsystem (32).

We apply the MUSCL approach for the nonlinear terms to obtain second order spatial discretisation. In what follows we analyse experimentally stability and convergence order of the above second order FV schemes. Test 1 and Test 3 in three space dimensions clearly shows the uniform stability as well as uniform second order convergence with respect to the singular parameter  $\varepsilon$ . This is due to the fact that the gravity/acoustic waves are not present in this experiment. In the consequent tests we have both the advective transport as well as the gravity/acoustic waves. Although we still have uniform stability, we will not be able to obtain the second order convergence uniformly with respect to  $\varepsilon$  unless our discretisation parameter  $\Delta x$  is sufficiently small to resolve the fast waves. This fact has been pointed out by Jin [28]: AP schemes are convergent uniformly with  $\varepsilon$ . If  $\varepsilon$  scales are resolved by discretization parameters  $\Delta x$ ,  $\Delta t$  of a particular scheme we get a good approximation of the limiting model, otherwise if  $\varepsilon$  is not resolved by discretization parameters a good approximation of the macroscopic model is obtained, see, e.g., [27], where this fact is confirmed also by theoretical analysis.

#### 6.1 Test 1: Traveling Vortex

Inspired by the exact solution of the 2D shallow water equations in [48] we adopt the traveling vortex test to the Euler equations. To this end we set  $p_0 = c_p = 2, c_v = 1, \ \theta = \overline{\theta} = 1$  and omit the gravity source term. Consequently,  $R = 1, \ \gamma = 2$  and  $p = \frac{1}{2}\rho^2$ . Then, the Euler equations (1) are analogous to the shallow water equations with a constant bottom topography. The acoustic/advection splitting yields for the pressure term  $p = p'_L + p'_{NL}, \quad p'_L = \overline{\rho}\rho', \quad p'_{NL} = \frac{1}{2}\rho'^2$  and coincides with the splitting in the shallow water equations [8, 7]. The initial data read

$$\rho(\mathbf{x}, 0) = 110 + \left(\frac{\Gamma \eta}{\omega}\right)^2 (k(\omega r) - k(\pi))\chi_{\omega r \le \pi}$$

$$u(\mathbf{x}, 0) = 0.6 + \Gamma(1 + \cos(\omega r))(0.5 - x_2)\chi_{\omega r \le \pi}$$

$$v(\mathbf{x}, 0) = \Gamma(1 + \cos(\omega r))(x_1 - 0.5)\chi_{\omega r \le \pi},$$

$$\theta(\mathbf{x}, 0) = \bar{\theta} = 1,$$
(62)

where  $r = \|\mathbf{x} - (0.5, 0.5)\|_2$ ,  $\Gamma = 1.5$ ,  $\omega = 4\pi$ ,  $k(r) = 2\cos(r) + 2r\sin(r) + \frac{\cos(2r)}{8} + \frac{r}{4}\sin(2r) + 0.75r^2$ . Here  $\Gamma$  is the so-called vortex intensity parameter,  $r_c$  the distance from the vortex core, and  $\omega$  an angular wave frequency that specifies the vortex width. Let us point out that the underlying equilibrium is constant due to the absence of gravity effects. More precisely,  $\bar{\rho} = \overline{\rho\theta} = 110$ . For the corresponding non-dimensional equation we have

$$\varepsilon = M = \frac{u_{ref}}{\sqrt{\rho_{ref}}} = \frac{0.6\eta}{\sqrt{110}} \tag{63}$$

and the Mach number can be controlled by adjusting the value of  $\eta$  in (63).

The computational domain is set to  $\Omega = [0, 1] \times [0, 1]$  and the periodic boundary conditions are used. The initial data are plotted in Figure 1. A rotating vortex, which is initially centered at (0.5, 0.5), is transported to the right with the velocity 0.6. Thus, the exact solution reads  $\mathbf{w}(\mathbf{x},t) = \mathbf{w}(\mathbf{x} - 0.6t, 0)$ . The numerical results obtained by the IMEX-ARS2 scheme for  $\varepsilon =$  $10^{-1}, 10^{-3}$  after one period, i.e. T = 5/3, are shown in Figures 2, 3. Tables 1, 2 show the  $L^1$ -errors and the experimental convergence rates (EOC) of the IMEX-ARS2 and IMEX-BDF2 schemes. We observe the second order convergence rates almost uniformly with respect to  $\varepsilon$ . Table 3 contains the convergence rates of the explicit EXP-RK2 scheme. For  $\varepsilon = 0.1$  the results of the traveling vortex test are similar for the considered explicit and IMEX schemes. However, the explicit scheme gives worse results in the asymptotic region, e.g., for  $\varepsilon = 10^{-3}$ , cf. Figure 4 and Table 3.



Figure 1: Traveling vortex test,  $\varepsilon = 0.1$ : initial data for  $\mathbf{w}_1 = \rho'$  (left/upper),  $\mathbf{w}_3 = (\rho \theta)'$  (left/lower),  $\mathbf{w}_{2,1} = \rho u$  (right/upper), and  $\mathbf{w}_{2,2} = \rho v$  (right/lower)



Figure 2: Traveling vortex test,  $\varepsilon = 0.1$ : numerical solution obtained by the IMEX-ARS2 scheme after one period (T = 5/3) for  $\mathbf{w}_1 = \rho'$  (left/upper),  $\mathbf{w}_3 = (\rho\theta)'$  (left/lower),  $\mathbf{w}_{2,1} = \rho u$  (right/upper), and  $\mathbf{w}_{2,2} = \rho v$  (right/lower).  $\Delta x_1 = \Delta x_2 = 1/160$ ,  $CFL_u = 0.45$ ,  $CFL \approx 3.8$ 



Figure 3: Traveling vortex test,  $\varepsilon = 0.001$ : numerical solution obtained by the IMEX-ARS2 scheme after one period (T = 5/3) for  $\mathbf{w}_1 = \rho'$  (left) and  $\mathbf{w}_{2,1} = \rho u$  (right).  $\Delta x_1 = \Delta x_2 = 1/160$ ,  $CFL_u = 0.45$ ,  $CFL \approx 339$ 



Figure 4: Traveling vortex test,  $\varepsilon = 0.001$ : numerical solution obtained by the EXP-RK2 scheme after one period (T = 5/3) for  $\mathbf{w}_1 = \rho'$  (left) and  $\mathbf{w}_{2,1} = \rho u$  (right).  $\Delta x_1 = \Delta x_2 = 1/160$ , CFL = 0.45

|     |   |             | ε =              | $= 10^{-1}, C$ | $FL \approx 3.8$   |         |                              |                     |  |  |  |  |
|-----|---|-------------|------------------|----------------|--------------------|---------|------------------------------|---------------------|--|--|--|--|
| Ν   | $L^1$ -error $\rho'$                      | EOC $\rho'$ | $L^1$ -error $m$ | EOC $m$        | $L^1$ -error $n$   | EOC $n$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |
| 10  | 3.889e-02                                 |             | 4.826e-01        |                | 7.477e-01          |         | 3.889e-02                    |                     |  |  |  |  |
| 20  | 9.341e-03                                 | 2.0576      | 1.247 e-01       | 1.9527         | 2.764e-01          | 1.4358  | 9.341e-03                    | 2.0576              |  |  |  |  |
| 40  | 3.209e-03                                 | 1.5414      | 3.699e-02        | 1.7528         | 7.098e-02          | 1.9613  | 3.209e-03                    | 1.5414              |  |  |  |  |
| 80  | 7.935e-04                                 | 2.0160      | 1.027e-02        | 1.8483         | 1.827 e-02         | 1.9578  | 7.935e-04                    | 2.0160              |  |  |  |  |
| 160 | 1.908e-04                                 | 2.0559      | 2.893e-03        | 1.8283         | 4.894e-03          | 1.9003  | 1.908e-04                    | 2.0559              |  |  |  |  |
|     | $\varepsilon = 10^{-3},  CFL \approx 339$ |             |                  |                |                    |         |                              |                     |  |  |  |  |
| Ν   | $L^1$ -error $\rho'$                      | EOC $\rho'$ | $L^1$ -error $m$ | EOC $m$        | $L^1$ -error $n$   | EOC $n$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |
| 10  | 7.554e-07                                 |             | 4.571e-01        |                | 7.742e-01          |         | 7.554e-07                    |                     |  |  |  |  |
| 20  | 1.993e-07                                 | 1.9223      | 1.240e-01        | 1.8825         | 2.634 e-01         | 1.5553  | 1.993e-07                    | 1.9223              |  |  |  |  |
| 40  | 4.597e-08                                 | 2.1162      | 3.241e-02        | 1.9357         | 6.691 e- 02        | 1.9772  | 4.597 e-08                   | 2.1162              |  |  |  |  |
| 80  | 1.300e-08                                 | 1.8219      | 9.076e-03        | 1.8362         | 1.732e-02          | 1.9496  | 1.300e-08                    | 1.8219              |  |  |  |  |
| 160 | 3.915e-09                                 | 1.7317      | 2.471e-03        | 1.8768         | 4.514e-03          | 1.9399  | 3.915e-09                    | 1.7317              |  |  |  |  |
|     |   |             | $\varepsilon =$  | $10^{-5}, CH$  | $FL \approx 33890$ |         |                              |                     |  |  |  |  |
| Ν   | $L^1$ -error $\rho'$                      | EOC $\rho'$ | $L^1$ -error $m$ | EOC $m$        | $L^1$ -error $n$   | EOC $n$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |
| 10  | 7.576e-11                                 |             | 4.571e-01        |                | 7.742e-01          |         | 7.576e-11                    |                     |  |  |  |  |
| 20  | 1.997e-11                                 | 1.9232      | 1.240e-01        | 1.8823         | 2.634 e-01         | 1.5552  | $1.997 e{-}11$               | 1.9232              |  |  |  |  |
| 40  | 4.854e-12                                 | 2.0409      | 3.241e-02        | 1.9356         | 6.691 e- 02        | 1.9772  | 4.854e-12                    | 2.0409              |  |  |  |  |
| 80  | 1.395e-12                                 | 1.7989      | 9.078e-03        | 1.8361         | 1.732e-02          | 1.9496  | 1.395e-12                    | 1.7989              |  |  |  |  |
| 160 | 5.132e-13                                 | 1.4426      | 2.472 e- 03      | 1.8766         | 4.515e-03          | 1.9399  | 5.132e-13                    | 1.4426              |  |  |  |  |

Table 1: Traveling vortex test: EOC for the IMEX-ARS2 scheme,  $CFL_u = 0.45, T = 0.1$ 

| -   |  |             |                  |               |                    |         |                              |                     |  |  |  |  |
|-----|--|-------------|------------------|---------------|--------------------|---------|------------------------------|---------------------|--|--|--|--|
| Ν   | $L^1$ -error $\rho'$                     | EOC $\rho'$ | $L^1$ -error $m$ | EOC $m$       | $L^1$ -error $n$   | EOC $n$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |
| 10  | 3.233e-02                                |             | 5.134e-01        |               | 7.980e-01          |         | 3.233e-02                    |                     |  |  |  |  |
| 20  | 4.958e-03                                | 2.7048      | 1.352e-01        | 1.9246        | 2.657 e-01         | 1.5865  | 4.958e-03                    | 2.7048              |  |  |  |  |
| 40  | 1.661e-03                                | 1.5779      | 3.610e-02        | 1.9057        | 7.202e-02          | 1.8834  | 1.661e-03                    | 1.5779              |  |  |  |  |
| 80  | 7.227e-04                                | 1.2004      | 9.992e-03        | 1.8531        | 1.886e-02          | 1.9334  | 7.227e-04                    | 1.2004              |  |  |  |  |
| 160 | 1.749e-04                                | 2.0468      | 2.863e-03        | 1.8034        | 5.074 e- 03        | 1.8937  | 1.749e-04                    | 2.0468              |  |  |  |  |
|     | $\varepsilon = 10^{-3}, CFL \approx 226$ |             |                  |               |                    |         |                              |                     |  |  |  |  |
| Ν   | $L^1$ -error $\rho'$                     | EOC $\rho'$ | $L^1$ -error $m$ | EOC $m$       | $L^1$ -error $n$   | EOC $n$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |
| 10  | 6.189e-07                                |             | 4.963e-01        |               | 7.948e-01          |         | 6.189e-07                    |                     |  |  |  |  |
| 20  | 1.777e-07                                | 1.8005      | 1.363e-01        | 1.8641        | 2.751e-01          | 1.5308  | 1.777e-07                    | 1.8005              |  |  |  |  |
| 40  | 4.900e-08                                | 1.8585      | 3.453e-02        | 1.9809        | 7.034e-02          | 1.9674  | 4.900e-08                    | 1.8585              |  |  |  |  |
| 80  | 1.270e-08                                | 1.9478      | 9.496e-03        | 1.8626        | 1.845 e- 02        | 1.9304  | 1.270e-08                    | 1.9478              |  |  |  |  |
| 160 | 3.299e-09                                | 1.9449      | 2.562e-03        | 1.8899        | 4.835e-03          | 1.9323  | 3.299e-09                    | 1.9449              |  |  |  |  |
|     |  |             | $\varepsilon =$  | $10^{-5}, CI$ | $FL \approx 22590$ |         |                              |                     |  |  |  |  |
| Ν   | $L^1$ -error $\rho'$                     | EOC $\rho'$ | $L^1$ -error $m$ | EOC $m$       | $L^1$ -error $n$   | EOC $n$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |
| 10  | 6.190e-11                                |             | 4.963e-01        |               | 7.948e-01          |         | 6.190e-11                    |                     |  |  |  |  |
| 20  | 1.777e-11                                | 1.8007      | 1.363e-01        | 1.8641        | 2.751e-01          | 1.5308  | 1.777e-11                    | 1.8007              |  |  |  |  |
| 40  | 4.900e-12                                | 1.8585      | 3.453 e-02       | 1.9809        | 7.034e-02          | 1.9674  | 4.900e-12                    | 1.8585              |  |  |  |  |
| 80  | 1.270e-12                                | 1.9481      | 9.496e-03        | 1.8627        | 1.845e-02          | 1.9305  | 1.270e-12                    | 1.9481              |  |  |  |  |
| 160 | 3.299e-13                                | 1.9446      | 2.562e-03        | 1.8899        | 4.835e-03          | 1.9324  | 3.298e-13                    | 1.9448              |  |  |  |  |

 $\varepsilon = 10^{-1}, CFL \approx 2.5$ 

Table 2: Traveling vortex test: EOC for the IMEX-BDF2 scheme,  $CFL_u = 0.3, T = 0.1$ 

|     | $\varepsilon = 10^{-1}$ |             |                  |                   |                  |         |                              |                     |  |  |  |  |  |
|-----|-------------------------|-------------|------------------|-------------------|------------------|---------|------------------------------|---------------------|--|--|--|--|--|
| Ν   | $L^1$ -error $\rho'$    | EOC $\rho'$ | $L^1$ -error $m$ | EOC $m$           | $L^1$ -error $n$ | EOC $n$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |  |
| 10  | 8.441e-03               |             | 1.484e + 00      |                   | 1.297e + 00      |         | 8.441e-03                    |                     |  |  |  |  |  |
| 20  | 5.412e-03               | 0.6413      | 7.834e-01        | 0.9215            | 8.015e-01        | 0.6944  | 5.412e-03                    | 0.6413              |  |  |  |  |  |
| 40  | 1.784e-03               | 1.6011      | 2.212e-01        | 1.8242            | 2.309e-01        | 1.7952  | 1.784e-03                    | 1.6011              |  |  |  |  |  |
| 80  | 4.163e-04               | 2.0993      | 4.593e-02        | 2.2681            | 4.832e-02        | 2.2568  | 4.163e-04                    | 2.0993              |  |  |  |  |  |
| 160 | 9.720e-05               | 2.0986      | 8.879e-03        | 2.3709            | 9.467 e-03       | 2.3516  | 9.720e-05                    | 2.0986              |  |  |  |  |  |
|     | $\varepsilon = 10^{-3}$ |             |                  |                   |                  |         |                              |                     |  |  |  |  |  |
| Ν   | $L^1$ -error $\rho'$    | EOC $\rho'$ | $L^1$ -error $m$ | EOC m             | $L^1$ -error $n$ | EOC $n$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |  |
| 10  | 7.509e-07               |             | 1.349e + 00      |                   | $1.221e{+}00$    |         | 7.509e-07                    |                     |  |  |  |  |  |
| 20  | 7.814e-07               | -0.0575     | 1.472e + 00      | -0.1266           | 1.464e + 00      | -0.2618 | 7.814e-07                    | -0.0575             |  |  |  |  |  |
| 40  | 8.515e-07               | -0.1239     | $1.731e{+}00$    | -0.2334           | $1.725e{+}00$    | -0.2367 | 8.515e-07                    | -0.1239             |  |  |  |  |  |
| 80  | 8.491e-07               | 0.0041      | 1.054e + 00      | 0.7160            | $1.053e{+}00$    | 0.7117  | 8.491e-07                    | 0.0041              |  |  |  |  |  |
| 160 | 7.176e-07               | 0.2427      | 3.258e-01        | 1.6935            | 3.258e-01        | 1.6928  | 7.176e-07                    | 0.2427              |  |  |  |  |  |
|     |                         |             |                  | $\varepsilon = 1$ | $0^{-5}$         |         |                              |                     |  |  |  |  |  |
| Ν   | $L^1$ -error $\rho'$    | EOC $\rho'$ | $L^1$ -error $m$ | EOC $m$           | $L^1$ -error $n$ | EOC $n$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |  |
| 10  | 7.508e-11               |             | 1.349e+00        |                   | 1.221e+00        |         | 7.508e-11                    |                     |  |  |  |  |  |
| 20  | 7.686e-11               | -0.0336     | 1.348e + 00      | 0.0009            | 1.339e + 00      | -0.1337 | 7.686e-11                    | -0.0336             |  |  |  |  |  |
| 40  | 7.728e-11               | -0.0079     | 1.348e + 00      | 0.0000            | 1.340e + 00      | -0.0000 | 7.728e-11                    | -0.0079             |  |  |  |  |  |
| 80  | 7.735e-11               | -0.0014     | 1.411e+00        | -0.0660           | 1.410e+00        | -0.0743 | 7.735e-11                    | -0.0014             |  |  |  |  |  |
| 160 | 1.310e-10               | -0.7597     | 1.725e + 00      | -0.2901           | $1.724e{+}00$    | -0.2901 | 1.310e-10                    | -0.7597             |  |  |  |  |  |

Table 3: Traveling vortex test: EOC for the EXP-RK2 scheme, CFL = 0.45, T = 0.1

### 6.2 Test 2: Colliding Pulses

We consider a weakly compressible flow test from [31] with the initial conditions

$$\rho = \bar{\rho} + \varepsilon \left( 1 - \cos \left( \frac{2\pi x}{L} \right) \right), \quad \bar{\rho} = 0.955$$
$$u = -\sqrt{\gamma} \operatorname{sgn}(x) \left( 1 - \cos \left( \frac{2\pi x}{L} \right) \right), \quad \gamma = 1.4$$
$$p = \bar{p} + \varepsilon \gamma \left( 1 - \cos \left( \frac{2\pi x}{L} \right) \right), \quad \overline{\rho \theta} = \bar{p} = 1, \ L = 2/\varepsilon$$

and the periodic boundary conditions. The computational domain is  $\Omega = [-L, L]$ . The initial data, see Figure 5, describe two acoustic pulses: one right-running pulse in the domain [-L, 0] and one left-running pulse in [0, L]. The two pulses collide and superimpose in the center of the domain. Their superposition at T = 0.815 is shown in Figure 6. Later the pulses separate and shock formation starts due to weakly nonlinear effects, cf. Figure 7 at T = 1.63. Analogous behaviour can be seen in Figures 8, 9 for  $\varepsilon = 0.001$ . Results computed by the IMEX-ARS2 scheme with the CFL numbers CFL = 0.45, 2, 4 coincide with the results obtained by the explicit EXP-RK2 scheme with CFL = 0.45.

Tables 4 and 5 show the EOC of the IMEX-BDF2 ( $CFL_u = 0.3$ ) and IMEX-ARS2 ( $CFL_u = 0.45$ ) schemes for  $\varepsilon = 0.1, 0.01, 0.001$ . Since the exact solution is not known, the reference solution is computed on a very fine mesh in order to evaluate the convergence rates (EOC). Note that the initial data are not well-prepared and there are fast acoustic waves present in the solution. As expected our IMEX schemes converge with the second order accuracy, but the convergence order can be recovered only on sufficiently fine meshes, so that fast acoustic waves can be resolved. Numerical experiments presented below confirm this fact.



Figure 5: Colliding pulses test,  $\varepsilon=1/11:$  initial data



Figure 6: Colliding pulses test,  $\varepsilon = 1/11$ : solutions obtained by the IMEX-ARS2 scheme with the CFL numbers CFL = 0.45, 2, 4 and by the EXP-RK2 scheme with CFL = 0.45 on a mesh with 400 cells at time T = 0.815



Figure 7: Colliding pulses test,  $\varepsilon = 1/11$ : solutions obtained by the IMEX-ARS2 scheme with the CFL numbers CFL = 0.45, 2, 4 and by the EXP-RK2 scheme with CFL = 0.45 on a mesh with 400 cells at time T = 1.63



Figure 8: Colliding pulses test,  $\varepsilon = 0.001$ : solutions obtained by the IMEX-ARS2 scheme with the CFL numbers CFL = 0.45, 2, 4 and by the EXP-RK2 scheme with CFL = 0.45 on a mesh with 400 cells at time T = 0.815

|  |                      |                   | ··-, ·           | = [ · ) -       | ]                            |                                  |  |  |  |  |
|--|----------------------|-------------------|------------------|-----------------|------------------------------|----------------------------------|--|--|--|--|
| Ν  | $L^1$ -error $\rho'$ | EOC $\rho'$       | $L^1$ -error $m$ | EOC $m$         | $L^1$ -error $(\rho\theta)'$ | $\overline{EOC} \ (\rho\theta)'$ |  |  |  |  |
| 40                                       | 2.509e-01            | 0.3070            | 3.11021          | 1.5760          | 2.632e-01                    | 0.3224                           |  |  |  |  |
| 80                                       | 7.290e-02            | 1.7829            | 0.99893          | 1.6386          | 7.607 e-02                   | 1.7906                           |  |  |  |  |
| 160                                      | 2.454e-02            | 1.5709            | 0.35623          | 1.4876          | 2.550e-02                    | 1.5765                           |  |  |  |  |
| 320                                      | 8.093e-03            | 1.6003            | 0.11577          | 1.6216          | 8.415e-03                    | 1.5997                           |  |  |  |  |
| 640                                      | 2.547 e-03           | 1.6680            | 0.03529          | 1.7138          | 2.647 e- 03                  | 1.6684                           |  |  |  |  |
| 1280                                     | 8.050e-04            | 1.6616            | 0.01130          | 1.6428          | 8.369e-04                    | 1.6614                           |  |  |  |  |
| 2560                                     | 2.366e-04            | 1.7667            | 0.00336          | 1.7495          | 2.463e-04                    | 1.7646                           |  |  |  |  |
| 5120                                     | 6.265 e- 05          | 1.9168            | 0.00090          | 1.9046          | 6.524 e- 05                  | 1.9166                           |  |  |  |  |
| $\varepsilon = 0.01,  CFL \in [22, 182]$ |                      |                   |                  |                 |                              |                                  |  |  |  |  |
| Ν  | $L^1$ -error $\rho'$ | EOC $\rho'$       | $L^1$ -error $m$ | EOC $m$         | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$              |  |  |  |  |
| 40                                       | 2.942e-02            | 2.2164            | 4.97053          | 1.9162          | 3.061e-02                    | 2.2178                           |  |  |  |  |
| 80                                       | 8.223e-01            | -4.8051           | 96.70602         | -4.2821         | 8.613e-01                    | -4.8144                          |  |  |  |  |
| 160                                      | 2.636e-01            | 1.6416            | 51.57914         | 0.9068          | 2.758e-01                    | 1.6427                           |  |  |  |  |
| 320                                      | 8.266e-02            | 1.6728            | 21.64870         | 1.2525          | 8.653 e-02                   | 1.6726                           |  |  |  |  |
| 640                                      | 2.298e-02            | 1.8470            | 7.29348          | 1.5696          | 2.405e-02                    | 1.8469                           |  |  |  |  |
| 1280                                     | 8.569e-03            | 1.4230            | 2.94300          | 1.3093          | 8.969e-03                    | 1.4231                           |  |  |  |  |
| 2560                                     | 2.659e-03            | 1.6886            | 0.86328          | 1.7694          | 2.782e-03                    | 1.6887                           |  |  |  |  |
| 5120                                     | 8.132e-04            | 1.7090            | 0.24643          | 1.8087          | 8.508e-04                    | 1.7094                           |  |  |  |  |
|  |                      | $\varepsilon = 0$ | 0.001, CFL       | $\in [229, 18]$ | 18]                          |                                  |  |  |  |  |
| Ν  | $L^1$ -error $\rho'$ | EOC $\rho'$       | $L^1$ -error $m$ | EOC $m$         | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$              |  |  |  |  |
| 640                                      | 6.551e-01            | 0.0000            | 756.54660        | 0.0000          | 6.860e-01                    | 0.0000                           |  |  |  |  |
| 1280                                     | 3.634 e-01           | 0.8504            | 608.20990        | 0.3149          | 3.805e-01                    | 0.8505                           |  |  |  |  |
| 2560                                     | 1.176e-01            | 1.6278            | 275.57173        | 1.1421          | 1.231e-01                    | 1.6279                           |  |  |  |  |
| 5120                                     | 3.525e-02            | 1.7377            | 111.27334        | 1.3083          | 3.691e-02                    | 1.7377                           |  |  |  |  |
| 10240                                    | 1.139e-02            | 1.6304            | 39.72628         | 1.4859          | 1.192e-02                    | 1.6304                           |  |  |  |  |
| 20480                                    | 3.620e-03            | 1.6534            | 13.07367         | 1.6034          | 3.790e-03                    | 1.6534                           |  |  |  |  |
| 40960                                    | 1.162e-03            | 1.6397            | 4.63654          | 1.4955          | 1.216e-03                    | 1.6397                           |  |  |  |  |
| 81920                                    | 3.689e-04            | 1.6549            | 1.20072          | 1.9492          | 3.862e-04                    | 1.6549                           |  |  |  |  |

 $\varepsilon = 0.1, CFL \in [2.7, 18]$ 

Table 4: Colliding pulses test: EOC for the IMEX-ARS2 scheme,  $CFL_u = 0.45, T = 0.815$ 

|       |  | $\varepsilon$ =   | = 0.1, CFL       | $\in [1.8, 12]$ |                              |                     |  |  |  |  |  |
|-------|--|-------------------|------------------|-----------------|------------------------------|---------------------|--|--|--|--|--|
| Ν     | $L^1$ -error $\rho'$                     | EOC $\rho'$       | $L^1$ -error $m$ | EOC $m$         | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |  |
| 40    | 2.447e-01                                | 0.8245            | 4.52910          | 1.2290          | 2.618e-01                    | 0.8518              |  |  |  |  |  |
| 80    | 1.376e-01                                | 0.8306            | 2.00780          | 1.1736          | 1.446e-01                    | 0.8562              |  |  |  |  |  |
| 160   | 6.051 e- 02                              | 1.1853            | 0.89010          | 1.1736          | 6.343e-02                    | 1.1889              |  |  |  |  |  |
| 320   | 1.949e-02                                | 1.6346            | 0.28626          | 1.6367          | 2.035e-02                    | 1.6403              |  |  |  |  |  |
| 640   | 6.319e-03                                | 1.6249            | 0.09305          | 1.6213          | 6.608e-03                    | 1.6226              |  |  |  |  |  |
| 1280  | 2.402e-03                                | 1.3957            | 0.03418          | 1.4448          | 2.524e-03                    | 1.3887              |  |  |  |  |  |
| 2560  | 7.247e-04                                | 1.7286            | 0.01012          | 1.7559          | 7.616e-04                    | 1.7284              |  |  |  |  |  |
| 5120  | 2.110e-04                                | 1.7801            | 0.00293          | 1.7875          | 2.220e-04                    | 1.7785              |  |  |  |  |  |
|       | $\varepsilon = 0.01,  CFL \in [15, 121]$ |                   |                  |                 |                              |                     |  |  |  |  |  |
| Ν     | $L^1$ -error $\rho'$                     | EOC $\rho'$       | $L^1$ -error $m$ | EOC $m$         | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |  |
| 40    | 3.277e-01                                | -1.2613           | 45.01215         | -1.2625         | 3.428e-01                    | -1.2674             |  |  |  |  |  |
| 80    | 1.758e-01                                | 0.8982            | 16.65396         | 1.4344          | 1.837 e-01                   | 0.9001              |  |  |  |  |  |
| 160   | 3.306e-01                                | -0.9111           | 51.31600         | -1.6235         | 3.465 e- 01                  | -0.9157             |  |  |  |  |  |
| 320   | 2.348e-01                                | 0.4937            | 39.51748         | 0.3769          | 2.459e-01                    | 0.4945              |  |  |  |  |  |
| 640   | 8.067e-02                                | 1.5414            | 17.58298         | 1.1683          | 8.448e-02                    | 1.5416              |  |  |  |  |  |
| 1280  | 2.651e-02                                | 1.6054            | 7.88240          | 1.1575          | 2.778e-02                    | 1.6045              |  |  |  |  |  |
| 2560  | 8.124e-03                                | 1.7062            | 2.90076          | 1.4422          | 8.511e-03                    | 1.7066              |  |  |  |  |  |
| 5120  | 2.557e-03                                | 1.6678            | 0.92974          | 1.6415          | 2.678e-03                    | 1.6684              |  |  |  |  |  |
|       |  | $\varepsilon = 0$ | 0.001, CFL       | $\in [153, 12]$ | 12]                          |                     |  |  |  |  |  |
| Ν     | $L^1$ -error $\rho'$                     | EOC $\rho'$       | $L^1$ -error $m$ | EOC $m$         | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |  |
| 640   | 1.577e-01                                | -0.9638           | 142.69328        | -0.7552         | 1.650e-01                    | -0.9632             |  |  |  |  |  |
| 1280  | 4.293e-01                                | -1.4448           | 669.35838        | -2.2299         | 4.495e-01                    | -1.4457             |  |  |  |  |  |
| 2560  | 3.149e-01                                | 0.4471            | 494.63460        | 0.4364          | 3.297 e-01                   | 0.4472              |  |  |  |  |  |
| 5120  | 1.151e-01                                | 1.4519            | 226.99826        | 1.1237          | 1.205e-01                    | 1.4519              |  |  |  |  |  |
| 10240 | 3.464 e- 02                              | 1.7322            | 97.06844         | 1.2256          | 3.628e-02                    | 1.7321              |  |  |  |  |  |
| 20480 | 1.007e-02                                | 1.7825            | 34.57141         | 1.4894          | 1.054 e-02                   | 1.7826              |  |  |  |  |  |
| 40960 | 3.566e-03                                | 1.4978            | 13.88341         | 1.3162          | 3.734e-03                    | 1.4978              |  |  |  |  |  |
| 81920 | 1.148e-03                                | 1.6345            | 4.44900          | 1.6418          | 1.203e-03                    | 1.6346              |  |  |  |  |  |

 $\varepsilon = 0.1, CFL \in [1.8, 12]$ 

Table 5: Colliding pulses test: EOC for the IMEX-BDF2 scheme,  $CFL_u = 0.45, T = 0.815$ 



Figure 9: Colliding pulses test,  $\varepsilon = 0.001$ : solutions obtained by the IMEX-ARS2 scheme with the CFL number CFL = 0.45 and by EXP-RK2 scheme with CFL = 0.45 on a mesh with 400 cells at time T = 1.63

### 6.3 Test 3: Free Convection of a Smooth Warm Air Bubble

In the following experiment we simulate free convection of a smooth warm air bubble (SWAB) proposed in [22], see also [42]. Initially, a warm air bubble is resting surrounded by cold air. Since the density of the warm air is lower, the bubble rises up due to the buoyancy force. The initial data are

$$\rho' = \frac{p_0}{R} \pi_e^{\frac{1}{\gamma - 1}} \left( \frac{1}{\theta} - \frac{1}{\bar{\theta}} \right) = -\bar{\rho} \frac{\theta'}{\theta}, \quad \pi_e = 1 - \frac{gy}{c_p \bar{\theta}}, \quad \bar{\rho} = \frac{p_0}{R \bar{\theta}} \pi_e^{\frac{1}{\gamma - 1}}$$

$$\mathbf{u} = 0$$

$$\theta' = \begin{cases} 0 & r > r_c \\ \frac{\theta'_c}{2} (1 + \cos\left(\frac{\pi r}{r_c}\right)) & r \le r_c \end{cases},$$
(64)

where  $\bar{\theta} = 300$ ,  $p_0 = \bar{p} = 10^5$ ,  $r_c = 250$ ,  $\theta'_c = 0.5$ ,  $r = \|\mathbf{x} - (500, 500, 350)^T\|_2$ . Note, that (64) implies that the initial perturbation  $(\rho\theta)' = 0$ , since  $(\rho\theta)' = \rho'\theta + \bar{\rho}\theta' = 0$ . Using the reference values  $x_{ref} = 1000$ m,  $t_{ref} = 1000$ s,  $u_{ref} = 1$ m/s,  $p_{ref} = R\rho_{ref}\theta_{ref}$  we have

$$\varepsilon^2 = \frac{u_{ref}^2}{x_{ref}g} = \frac{u_{ref}^2 \rho_{ref}}{p_{ref}} = \frac{u_{ref}^2}{R\theta_{ref}}$$

and consequently  $\theta_{ref} = \frac{u_{ref}^2}{R\varepsilon^2} = \varepsilon^{-2}/R$ . Thus, the non-dimensional initial data read

$$\theta' = \begin{cases} 0 & r > r_c \\ \frac{\theta'_c}{2} \left(1 + \cos\left(\frac{\pi r}{r_c}\right)\right) & r \le r_c \end{cases}, \quad r = \|\mathbf{x} - (0.5, 0.5, 0.35)^T\|_2, \\ r_c = 0.25, \quad \theta'_c = \frac{1}{2\theta_{ref}} = \frac{R\varepsilon^2}{2}, \\ \rho' = -\frac{\bar{\rho}\theta'}{\theta}, \quad \bar{\theta} = 1, \quad \bar{\rho} = \left(1 - \frac{\gamma - 1}{\gamma}x_3\right)^{\frac{1}{\gamma - 1}}. \end{cases}$$
(65)

In this experiment it is reasonable to apply no-flux boundary conditions  $\mathbf{u} \cdot \mathbf{n} = 0$ ,  $\nabla(\bar{c}^2(\rho\theta)') \cdot \mathbf{n} = 0$ ,  $\nabla\rho' \cdot \mathbf{n} = 0$ . Note, that these boundary conditions are reflected in the system matrix A in (29) and most importantly in the matrix E in (32). Let us highlight the fact that different boundary conditions are used for  $\mathbf{u}$  and  $(\rho\theta)'$ ,  $\rho'$ , respectively, by  $\mathfrak{D}_{x_j}^u$  and  $\mathfrak{D}_{x_j}^p$ , j = 1, 2, 3. Consequently, we have the following discrete equations for the momentum, cf. (31)

$$\mathbf{Q}_{j}^{n+1} = \hat{\mathbf{Q}} - \frac{\Delta t}{\varepsilon^{2}} \mathfrak{D}_{x_{j}}^{p} \bar{C}^{2} \bar{\Theta}^{-1} (\boldsymbol{\rho} \boldsymbol{\theta})^{\prime n+1}, \quad j = 1, 2, \\ \mathbf{Q}_{3}^{n+1} = \hat{\mathbf{Q}} - \frac{\Delta t}{\varepsilon^{2}} \mathfrak{D}_{x_{3}}^{p} \bar{C}^{2} \bar{\Theta}^{-1} (\boldsymbol{\rho} \boldsymbol{\theta})^{\prime n+1} - \frac{\Delta t}{\varepsilon^{2}} \boldsymbol{\rho}^{\prime n+1}$$

and for the potential temperature, cf. (32)

$$\left[\mathbb{1} - \frac{\Delta t^2}{\varepsilon^2} E\right] (\boldsymbol{\rho}\boldsymbol{\theta})^{\prime n+1} = (\hat{\boldsymbol{\rho}\boldsymbol{\theta}})^{\prime} - \Delta t \bar{\Theta} \nabla_h^u \cdot \hat{\mathbf{Q}} - \frac{\Delta t^2}{\varepsilon^2} \mathfrak{D}_{x_3}^u ((\hat{\boldsymbol{\rho}\boldsymbol{\theta}})^{\prime} - \bar{\Theta} \boldsymbol{\rho}^{\prime}), \tag{66}$$

where

$$E = \Delta_h^p \bar{C}^2 + \mathfrak{D}_{x_3}^u, \quad \Delta_h^p = \sum_{i=1}^3 \mathfrak{D}_{x_i}^u \mathfrak{D}_{x_i}^p.$$
(67)

#### 6.3.1 One-dimensional case

Firstly, we consider one-dimensional setting, which allows us to compute a numerical solution using sufficiently fine mesh resolution. We set the computational domain  $\Omega$  to [0, 1], place the center of warm air bubble at x = 0.5 and use no-flux boundary conditions. The solution shows the following behaviour: in the beginning the potential temperature and velocity evolve quite rapidly, while the density is changing only slowly. Then the solution changes in a periodic pattern on a fast time scale. Let us note that the solution dynamics in one space dimension differs substantially from the multi-dimensional situation. Nevertheless, we can use this test case to analyse the accuracy and the experimental order of convergence with respect to  $\varepsilon$  and CFLnumbers. Due to the presence of the fast waves we obtain the second order convergence rates only for relatively fine grids if the  $CFL_u$  stability condition (25) is used, see Tables 6 and 7. On the other hand, Tables 8 and 9 demonstrate that under a slight control of the whole CFL number (26), e.g. CFL = 8, the second order accuracy can be recovered on coarser meshes. In Tables 7 and 9 we present the experimental order of convergence using the weighted norms  $\|\bar{c}\rho'/\varepsilon\|_{L^2(\Omega)}$ ,  $\|m\|_{L^2(\Omega)}$  and  $\|\bar{c}(\rho\theta)'/(\bar{\theta}\varepsilon)\|_{L^2(\Omega)}$  that follows from the stability analysis, cf. Section 5. We can clearly notice higher convergence rates with respect to these energy-related norms.

### 6.3.2 Multi-dimensional case

In this experiment we will consider three-dimensional rising air bubble test (64). The initial data and the numerical solution obtained by the three-dimensional simulations using the IMEX-

|        |                      |             | $\varepsilon = 0.0$  | 1       |                              |                     |
|--------|----------------------|-------------|----------------------|---------|------------------------------|---------------------|
| Ν      | $L^1$ -error $\rho'$ | EOC $\rho'$ | $L^1$ -error $m$     | EOC $m$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |
| 640    | 2.880e-04            | 0.1456      | 3.990e-03            | 2.3115  | 2.912e-04                    | 0.1436              |
| 1280   | 9.598e-05            | 1.5853      | 1.619e-02            | -2.0207 | 9.611e-05                    | 1.5993              |
| 2560   | 4.233e-05            | 1.1812      | 6.076e-03            | 1.4138  | 4.236e-05                    | 1.1819              |
| 5120   | 1.307e-05            | 1.6948      | 1.267 e-03           | 2.2620  | 1.309e-05                    | 1.6946              |
| 10240  | 3.552e-06            | 1.8799      | 2.764 e- 04          | 2.1965  | 3.554 e- 06                  | 1.8808              |
| 20480  | 8.899e-07            | 1.9970      | 6.526e-05            | 2.0823  | 8.901e-07                    | 1.9974              |
|        |                      |             | $\varepsilon = 0.00$ | )1      |                              |                     |
| Ν      | $L^1$ -error $\rho'$ | EOC $\rho'$ | $L^1$ -error $m$     | EOC $m$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |
| 10240  | 1.736e-06            | 2.8347      | 5.040e-03            | -0.5310 | 1.736e-06                    | 2.8348              |
| 20480  | 1.153e-06            | 0.5907      | 3.316e-03            | 0.6039  | 1.153e-06                    | 0.5906              |
| 40960  | 1.620e-06            | -0.4914     | 1.124e-03            | 1.5610  | 1.621e-06                    | -0.4915             |
| 81920  | 4.354e-07            | 1.8959      | 5.439e-04            | 1.0471  | 4.354e-07                    | 1.8960              |
| 163840 | 6.547 e-08           | 2.7335      | 1.654 e- 04          | 1.7176  | 6.547 e-08                   | 2.7334              |
| 327680 | 1.873e-08            | 1.8058      | 4.274e-05            | 1.9521  | 1.873e-08                    | 1.8058              |

Table 6: SWAB 1D test: EOC for the IMEX-ARS2 scheme,  $CFL_u = 0.45, T = 0.05$ 

|        | $\varepsilon = 0.01$                    |        |                      |         |   |        |  |  |  |  |  |  |
|--------|---|--------|----------------------|---------|---|--------|--|--|--|--|--|--|
| Ν      | $L^2$ -error $\bar{c}\rho'/\varepsilon$ | EOC    | $L^2$ -error $m$     | EOC     | $L^2$ -error $\bar{c}(\rho\theta)'/(\bar{\theta}\varepsilon)$ | EOC    |  |  |  |  |  |  |
| 640    | 1.439e-03                               | 0.8225 | 1.842e-04            | 2.8751  | 1.455e-03   | 0.8091 |  |  |  |  |  |  |
| 1280   | 3.243e-04                               | 2.1495 | 5.206e-04            | -1.4986 | 3.249e-04   | 2.1630 |  |  |  |  |  |  |
| 2560   | 1.070e-04                               | 1.6001 | 1.400e-04            | 1.8951  | 1.070e-04   | 1.6022 |  |  |  |  |  |  |
| 5120   | 2.567 e-05                              | 2.0593 | 2.481e-05            | 2.4960  | 2.567 e- 05   | 2.0594 |  |  |  |  |  |  |
| 10240  | 5.075e-06                               | 2.3385 | 4.172e-06            | 2.5721  | 5.075e-06   | 2.3387 |  |  |  |  |  |  |
| 20480  | 9.306e-07                               | 2.4473 | 7.261e-07            | 2.5226  | 9.306e-07   | 2.4473 |  |  |  |  |  |  |
|        |   |        | $\varepsilon = 0.00$ | 1       |   |        |  |  |  |  |  |  |
| Ν      | $L^2$ -error $\bar{c}\rho'/\varepsilon$ | EOC    | $L^2$ -error $m$     | EOC     | $L^2$ -error $\bar{c}(\rho\theta)'/(\bar{\theta}\varepsilon)$ | EOC    |  |  |  |  |  |  |
| 10240  | 1.979e-05                               | 3.1364 | 5.239e-05            | 0.0156  | 1.979e-05   | 3.1365 |  |  |  |  |  |  |
| 20480  | 8.333e-06                               | 1.2480 | 2.690e-05            | 0.9614  | 8.334e-06   | 1.2479 |  |  |  |  |  |  |
| 40960  | 8.121e-06                               | 0.0372 | 6.512e-06            | 2.0468  | 8.122e-06   | 0.0372 |  |  |  |  |  |  |
| 81920  | 1.663e-06                               | 2.2878 | 2.503e-06            | 1.3794  | 1.663 e-06  | 2.2879 |  |  |  |  |  |  |
| 163840 | 1.938e-07                               | 3.1012 | 5.716e-07            | 2.1304  | 1.938e-07   | 3.1012 |  |  |  |  |  |  |
| 327680 | 3.855e-08                               | 2.3297 | 1.020e-07            | 2.4870  | 3.855e-08   | 2.3297 |  |  |  |  |  |  |

Table 7: SWAB 1D test: EOC for the IMEX-ARS2 scheme,  $CFL_u = 0.45, T = 0.05$ 

|      | 0 0.01, 01 2 0                 |             |                  |         |                              |                     |  |  |  |  |  |  |
|------|--------------------------------|-------------|------------------|---------|------------------------------|---------------------|--|--|--|--|--|--|
| Ν    | $L^1$ -error $\rho'$           | EOC $\rho'$ | $L^1$ -error $m$ | EOC $m$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |  |  |
| 320  | 1.680e-05                      | 1.6495      | 1.654 e-03       | 2.1858  | 1.680e-05                    | 1.6534              |  |  |  |  |  |  |
| 640  | 4.470e-06                      | 1.9102      | 3.777e-04        | 2.1309  | 4.468e-06                    | 1.9113              |  |  |  |  |  |  |
| 1280 | 1.148e-06                      | 1.9613      | 9.155e-05        | 2.0446  | 1.148e-06                    | 1.9608              |  |  |  |  |  |  |
| 2560 | 2.846e-07                      | 2.0121      | 2.237 e-05       | 2.0330  | 2.844e-07                    | 2.0126              |  |  |  |  |  |  |
| 5120 | 7.009e-08                      | 2.0215      | 5.852 e-06       | 1.9344  | 6.994 e- 08                  | 2.0239              |  |  |  |  |  |  |
|      | $\varepsilon = 0.001, CFL = 8$ |             |                  |         |                              |                     |  |  |  |  |  |  |
| Ν    | $L^1$ -error $\rho'$           | EOC $\rho'$ | $L^1$ -error $m$ | EOC $m$ | $L^1$ -error $(\rho\theta)'$ | EOC $(\rho\theta)'$ |  |  |  |  |  |  |
| 320  | 1.177e-06                      | -0.4086     | 1.645e-03        | 1.3203  | 1.177e-06                    | -0.4083             |  |  |  |  |  |  |
| 640  | 2.954e-07                      | 1.9942      | 6.658e-04        | 1.3048  | 2.954e-07                    | 1.9942              |  |  |  |  |  |  |
| 1280 | 5.906e-08                      | 2.3225      | 2.236e-04        | 1.5744  | 5.907 e-08                   | 2.3224              |  |  |  |  |  |  |
| 2560 | 1.686e-08                      | 1.8087      | 6.226e-05        | 1.8445  | 1.686e-08                    | 1.8089              |  |  |  |  |  |  |
| 5120 | 4.245e-09                      | 1.9898      | 1.616e-05        | 1.9461  | 4.244 e-09                   | 1.9898              |  |  |  |  |  |  |

 $\varepsilon = 0.01, CFL = 8$ 

Table 8: SWAB 1D test: EOC for the IMEX-ARS2 scheme,  $T=\ 0.05$ 

|      | $\varepsilon = 0.01$                    |        |                      |        |   |        |  |  |  |  |  |  |
|------|---|--------|----------------------|--------|---|--------|--|--|--|--|--|--|
| Ν    | $L^2$ -error $\bar{c}\rho'/\varepsilon$ | EOC    | $L^2$ -error $m$     | EOC    | $L^2$ -error $\bar{c}(\rho\theta)'/(\bar{\theta}\varepsilon)$ | EOC    |  |  |  |  |  |  |
| 320  | 1.264e-04                               | 2.0085 | 1.275e-04            | 2.4349 | 1.264 e-04  | 2.0130 |  |  |  |  |  |  |
| 640  | 2.551e-05                               | 2.3095 | 2.170e-05            | 2.5545 | 2.549e-05   | 2.3098 |  |  |  |  |  |  |
| 1280 | 4.767e-06                               | 2.4197 | 3.817e-06            | 2.5076 | 4.764 e-06  | 2.4196 |  |  |  |  |  |  |
| 2560 | 8.765e-07                               | 2.4434 | 6.970 e- 07          | 2.4531 | 8.758e-07   | 2.4434 |  |  |  |  |  |  |
| 5120 | 1.630e-07                               | 2.4271 | 1.327 e-07           | 2.3934 | 1.629e-07   | 2.4271 |  |  |  |  |  |  |
|      |   |        | $\varepsilon = 0.00$ | )1     |   |        |  |  |  |  |  |  |
| Ν    | $L^2$ -error $\bar{c}\rho'/\varepsilon$ | EOC    | $L^2$ -error $m$     | EOC    | $L^2$ -error $\bar{c}(\rho\theta)'/(\bar{\theta}\varepsilon)$ | EOC    |  |  |  |  |  |  |
| 320  | 8.082e-05                               | 0.1267 | 1.126e-04            | 1.8214 | 8.082e-05   | 0.1272 |  |  |  |  |  |  |
| 640  | 1.667 e-05                              | 2.2772 | 3.234e-05            | 1.7995 | 1.667 e-05  | 2.2772 |  |  |  |  |  |  |
| 1280 | 2.249e-06                               | 2.8899 | 7.249e-06            | 2.1575 | 2.250e-06   | 2.8898 |  |  |  |  |  |  |
| 2560 | 4.542 e- 07                             | 2.3081 | 1.395e-06            | 2.3770 | 4.543e-07   | 2.3081 |  |  |  |  |  |  |
| 5120 | 8.606e-08                               | 2.4000 | 2.542 e- 07          | 2.4568 | 8.606e-08   | 2.4001 |  |  |  |  |  |  |

Table 9: SWAB 1D test: EOC for the IMEX-ARS2 scheme,  $CFL=8,\,T=~0.05$ 

| N   | $L^1$ -error <b>w</b> | EOC $\mathbf{w}$ | $L^1$ -error $m_1$ | EOC $m_1$ | $L^1$ -error $m_3$ | EOC $m_3$ | $L^1$ -error $\theta'$ | EOC $\theta'$ |
|-----|-----------------------|------------------|--------------------|-----------|--------------------|-----------|------------------------|---------------|
| 32  | 3.296e-03             | 2.0487           | 6.662 e- 03        | 2.0944    | 6.480e-03          | 2.0025    | 1.809e-03              | 1.6086        |
| 64  | 7.967e-04             | 2.0194           | 1.560e-03          | 2.0152    | 1.617e-03          | 2.0248    | 5.932e-04              | 1.7868        |
| 128 | 1.965e-04             | 1.8050           | 3.859e-04          | 1.7343    | 3.974e-04          | 1.8836    | 1.719e-04              | 2.0539        |
| 256 | 5.624 e- 05           | 1.9046           | 1.160e-04          | 1.9570    | 1.077e-04          | 1.8810    | 4.140e-05              | 2.0227        |
| 512 | 1.502e-05             | 1.3961           | 2.987 e-05         | 1.8213    | 2.924e-05          | 1.1223    | 1.019e-05              | 2.3914        |

Table 10: SWAB quasi-3D test: EOC of IMEX-BDF2 scheme, T = 0.15,  $CFL_u = 0.4$ ,  $CFL \in [2.8, 300]$ ,  $\varepsilon = 0.01$ .

| N   | $L^1$ -error <b>w</b> | EOC $\mathbf{w}$ | $L^1$ -error $m_1$ | EOC $m_1$ | $L^1$ -error $m_3$ | EOC $m_3$ | $L^1$ -error $\theta'$ | EOC $\theta'$ |
|-----|-----------------------|------------------|--------------------|-----------|--------------------|-----------|------------------------|---------------|
| 32  | 9.470e-03             | 1.0416           | 1.862e-02          | 1.0563    | 1.859e-02          | 1.0673    | 1.556e-03              | 0.9429        |
| 64  | 4.601e-03             | 0.9944           | 8.953e-03          | 1.0304    | 8.871e-03          | 1.0396    | 8.094e-04              | 1.0475        |
| 128 | 2.309e-03             | 0.9993           | 4.383e-03          | 1.0949    | 4.315e-03          | 1.0823    | 3.916e-04              | 1.1047        |
| 256 | 1.155e-03             | 0.9381           | 2.052e-03          | 1.2167    | 2.038e-03          | 1.0339    | 1.821e-04              | 1.2251        |
| 512 | 6.029e-04             | 0.8246           | 8.830e-04          | 1.5853    | 9.953e-04          | 1.2301    | 7.790e-05              | 1.5804        |

Table 11: SWAB quasi-3D test: EOC of IMEX-ARS2 scheme, T = 0.15,  $CFL_u = 0.4$ ,  $CFL \in [2.8, 300]$ ,  $\varepsilon = 0.01$ .

BDF2 scheme are shown in Figure 10. In tables Table 10 and 11 the experimental order of convergence was obtained by means of quasi-3D simulations, see Figure 11. To reduce CPU time these experiments were performed in a 3D-box in which the  $x_2$ -direction consists of one layer of cells whereas each of the  $x_1$  and  $x_3$  directions consists of N layers of cells. Numerical experiments clearly demonstrate the expected second order accuracy even on relatively coarse grids for the IMEX-BDF2 scheme. Note that the convergence of the IMEX-ARS2 scheme is slightly worse for this test case, as shown in Table 11.

### 6.4 Test 4: Inertia-gravity waves

The inertia-gravity waves experiment has been taken from [22]. The initial conditions have been proposed firstly in [53]. The background state is a uniformly stratified atmosphere with a Brunt-Väisälä frequency

$$\mathcal{N} = g \frac{d}{dy} (\ln \bar{\theta})$$

which yields the background potential temperature

$$\bar{\theta} = \theta_0 \exp\left(\frac{\mathcal{N}^2}{g}y\right).$$

The Exner pressure obtained from the hydrostatic balance yields in this case

$$\bar{\pi} = 1 + \frac{g^2}{c_p \theta_0 \mathcal{N}^2} \left( \exp\left(-\frac{\mathcal{N}^2}{g}y\right) - 1 \right).$$

The perturbation of the potential temperature is given by



Figure 10: SWAB 3D test,  $\varepsilon = 0.01$ : IMEX-BDF2 scheme, for times (from left to right, top to bottom) t = 0, 0.3, 0.5, 0.6, 0.7, 1.1, with mesh resolution  $\Delta x_1 = \Delta x_2 = \Delta x_3 = 1/128$ ,  $CFL_u = 0.4, CFL \in [27, 200]$ . Only a half of the computational domain is shown in the  $x_1$ -direction to visualize the interior temperature profiles. Colors correspond to the potential temperature  $\theta'$  in the range 0 - 0.1K. The background color ( $\theta' = 0$ ) has been removed.



Figure 11: SWAB quasi-3D test,  $\varepsilon = 0.01$ : IMEX-BDF2 scheme, for times (from left to right, top to bottom) t = 0, 0.3, 0.5, 0.6, 0.7, 1.1, with mesh resolution  $\Delta x_1 = \Delta x_2 = \Delta x_3 = 1/128$ ,  $CFL_u = 0.4, CFL \in [27, 200]$ . The  $x_1 - x_3$  planes illustrate time evolution of the interior temperature profiles of a three-dimensional system containing one cell layer in the  $x_2$ -direction. Colors correspond to the potential temperature  $\theta'$  in the range 0 - 0.5K.

$$\theta' = \theta_c \frac{\sin\left(\frac{\pi_c y}{h_c}\right)}{1 + \left(\frac{x - x_c}{a_c}\right)^2},$$

where  $\theta_c = 0.01$ K,  $\theta_0 = 300$ K,  $h_c = 10$ km,  $a_c = 5$ km,  $x_c = 100$ km, and  $\mathcal{N} = 0.01$ s<sup>-1</sup>. The domain size in the  $(x_1, x_2, x_3)$  directions is 300km×0.25km×10km. We use periodic and no-flux boundary conditions for the horizontal and vertical directions, respectively. This initial state is advected horizontally with a constant velocity  $\bar{u} = 20$ m/s.

Figure 12 shows the excess potential temperature for the Lax-Friedrichs flux models obtained after 3000s on regular grids with the resolution 250m calculated using dimensional formulation of the Euler equations (4). The global extreme values of the results are in the range  $\theta' =$ [-0.001772, 0.003379] and w = [-0.0102006, 0.014102]. The result demonstrates that the IMEX finite volume method can be successfully applied to compute internal gravity waves in the non-homentropic case, that is, when the background potential temperature is non-constant. Note that the results with/without the non-linear pressure perturbation  $p'_{NL}$  are similar (see Figure 12).



Figure 12: Inertia-gravity wave quasi-3D test using the Euler equations (4) with  $\varepsilon \approx 0.06$  computed by the IMEX-ARS2 method with the Lax-Friedrichs flux. Top: initial data for the potential temperature  $\theta'$ ; middle:  $\theta'$  at time t = 3000s using only the linear pressure perturbation,  $p'_L$ ; bottom:  $\theta'$  at time t = 3000s using also the non-linear pressure perturbation,  $p'_{NL}$ , in the non-linear operator. Mesh resolution  $\Delta x_1 = \Delta x_2 = \Delta x_3 = 1/4$ ,  $CFL_u = 0.4$ ,  $CFL \approx 7$ . Colors correspond to the potential temperature  $\theta'$  in the range [-0.003 0.003]K, contour levels are shown for the values [-0.0015 0.003]K by the step 0.0005K.

# 7 Conclusions

In the present paper we have derived and analysed asymptotic preserving IMEX FV methods for low Mach number flows with gravitation. The compressible Euler equations (1) are governed by hyperbolic balance laws describing the evolution of density, momentum and potential temperature. This system is often used in meteorology in order to model stratified fluid flows. In the low Mach number regime, which is typical for meteorological applications, the resulting system has a multiscale character. In order to efficiently approximate slow advective flows, we split the full nonlinear system into the linear and nonlinear operators. The stiff linear operator models the linearized acoustic and gravity waves, whereas the non-stiff nonlinear operator represents the advective transport. For spatial discretization we apply the finite volume method with suitable numerical fluxes. Thus, to avoid numerical diffusion in the linear waves the central difference fluxes are used. On the other hand, we can apply any suitable numerical flux, that is used for hyperbolic conservation laws, in order to approximate the nonlinear operator. In this paper we have used the Rusanov or the Lax-Friedrichs method. For time discretization second order globally stiffly accurate IMEX methods are applied: the stiff linear operator is approximated implicitly and the nonlinear non-stiff operator explicitly in time.

In Sections 4 and 5 we have proved that the proposed IMEX FV methods are asymptotic preserving in the sense that they are uniformly consistent and stable for any  $0 < \varepsilon << 1$ . Moreover, our schemes preserve the hydrostatic equilibrium state in the following sense: if  $\mathbf{w}^n = \mathbf{0}$ , then also  $\mathbf{w}^{n+1} = \mathbf{0}$ . Consequently, they are also well-balanced. A series of one-, two-and three-dimensional numerical experiments confirm the asymptotic preserving property of the derived IMEX FV schemes. Indeed, if the advective effects are dominant we obtain the second order convergence rate uniformly with respect to  $\varepsilon$ .

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